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Transformarea Energetică și Calitatea Mediului Interior a Clădirilor

În contextul actual, în care eficiența energetică și sustenabilitatea sunt priorități globale, respectarea reglementărilor tehnice și legale devine esențială. Unul dintre articolele din acest număr își propune să sublinieze importanța respectării reglementării tehnice Mc001/2022 și a legii 372 în România, ambele având ca scop îmbunătățirea performanței energetice a clădirilor.

Reglementarea tehnică Mc001/2022 vine să actualizeze normele anterioare, introducând criterii mai stricte pentru eficiența energetică și calitatea materialelor de construcție. Legea 372, pe de altă parte, stabilește cadrul general pentru evaluarea performanței energetice a clădirilor, inclusiv certificarea energetică și auditurile energetice. Conformitatea cu Mc001/2022 și Legea 372 contribuie la reducerea emisiilor de CO₂ și la atingerea obiectivelor de sustenabilitate ale țării. De asemenea, îmbunătățește calitatea vieții ocupanților prin crearea unui mediu interior mai sănătos și confortabil. Respectarea reglementării tehnice Mc001/2022 și a legii 372 nu este doar o obligație legală, ci și o responsabilitate etică și socială. Aceasta reprezintă un pas esențial în direcția unui viitor mai susținabil și a unei calități mai bune a vieții pentru toți cetățenii.

Alte informații utile se regăsesc în revistă și se discută politicele UE în materie de energie curată și modul în care acestea pot fi implementate cu succes la nivel național. Articolele publicate în acest număr subliniază importanța dezvoltării competențelor în digitalizare, respectarea normelor și importanța calității mediului interior.

Lectură plăcută și pe curând la
Conferința Națională AIIR - 12-13 Octombrie 2023, Brașov!

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Importanța respectării reglementării tehnice Mc001/2022 și a legii 372 privind performanța energetică a clădirilor



Comunicat de presă

Cătălin Lungu¹

¹Președinte REHVA
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Comisia Europeană a propus în iulie 2021 pachetul legislativ "Fit for 55" pentru a atinge obiectivele de mediu stabilite în cadrul Acordului Verde European. Propunerile includ o reducere a emisiilor de gaze cu efect de seră cu cel puțin 55% până în 2030, comparativ cu nivelurile din 1990. Aceste măsuri au scopul de a face economia UE mai sustenabilă și mai prietenoasă cu mediul înconjurător.



Ministerul Dezvoltării Lucrărilor Publice și Administrației (M.D.L.P.A.) a actualizat în ultimii 2 ani numeroase norme tehnice aferente sectorului clădirilor pentru a adapta baza legală utilizată de toți operatorii din domeniul construcțiilor (autorități locale și instituționale, auditori energetici pentru clădiri și proiectanți, execuțanți, dezvoltatori imobiliari, agenții imobiliare, beneficiari etc.) în vederea încadrării, în anii următori, în întele de mediu angajate de Guvernul României.

Astfel, conform Ordinului M.D.L.P.A. nr. 16/2023, apărut în Monitorul Oficial nr. 46 din 17 ianuarie 2023, reglementarea tehnică "Metodologie de calcul al performanței energetice a clădirilor, indicativ Mc 001-2022" a intrat integral în vigoare la 17 iulie 2023 (detalii pe www.oaer.ro).

Odată cu această reglementare, apar noutăți importante în privința autorizării clădirilor noi și a celor existente care se renovează.

Mai jos sunt listate o parte din aceste noutăți pentru ca toți actorii care lucrează în domeniul construcțiilor de clădiri să fie informați și să analizeze ulterior în detaliu prevederile tehnice din Mc001-2022:

1) pentru autorizarea clădirilor noi trebuie să fie menționată în certificatele de urbanism cerința obligatorie privind întocmirea Raportului de Conformare NZEB (Nearly Zero Energy Building) prin care proiectantul încadrează clădirea nouă pe care o proiectează în categoria clădirilor cu consum de energie aproape de zero, arătând cum sunt respectate condițiile privind (1) consumul maxim de energie, (2) emisiile de CO₂ aferente consumului total de energie și (3) procentul minim de 30% de energie consumată din sursele regenerabile;

2) pentru autorizarea tuturor clădirilor noi sau existente care se renovează, trebuie să fie menționată în certificatele de urbanism, dacă se utilizează fonduri publice, cerința obligatorie pentru întocmirea de către proiectant a Studiului privind Fezabilitatea din punct de vedere tehnic, economic și al mediului înconjurator a utilizării sistemelor alternative de înaltă eficiență;

3) s-a modificat integral forma certificatului de performanță energetică, valorile care definesc clasele de performanță energetică și de mediu fiind diferite în funcție de categoria de clădire;

4) certificatele de performanță energetică nu sunt valabile fără codul unic de înregistrare și este interzisă utilizarea lor de către proprietari/administratori/beneficiari/dezvoltatorii clădirilor/unităților de clădire/apartamentelor;

5) calculul coeficientului global de izolare termică devine de importanță secundară, în consecință nu este necesar să mai apară ca cerință în Certificatele de Urbanism, consumul energetic calculat cu Mc001-2022 fiind acum cerința de performanță energetică;

6) rezistențele termice ale elementelor de construcție nu mai au valori impuse, cele prezentate în Mc001-2022 fiind valori recomandate pentru atingerea unui consum calculat al clădirii sub cel maxim admis;

7) sistemele de ventilare mecanică devin obligatorii pentru toate clădirile nerezidențiale noi sau existente care se renovează;

8) s-a modificat procedura de calcul a consumurilor de energie consumată de clădiri pentru încălzire, răcire, ventilare, apă caldă de consum și iluminat.



Pentru autorizarea clădirilor existente care se renoviază, întocmirea Raportului de Audit Energetic se păstrează ca cerință obligatorie în certificatele de urbanism.

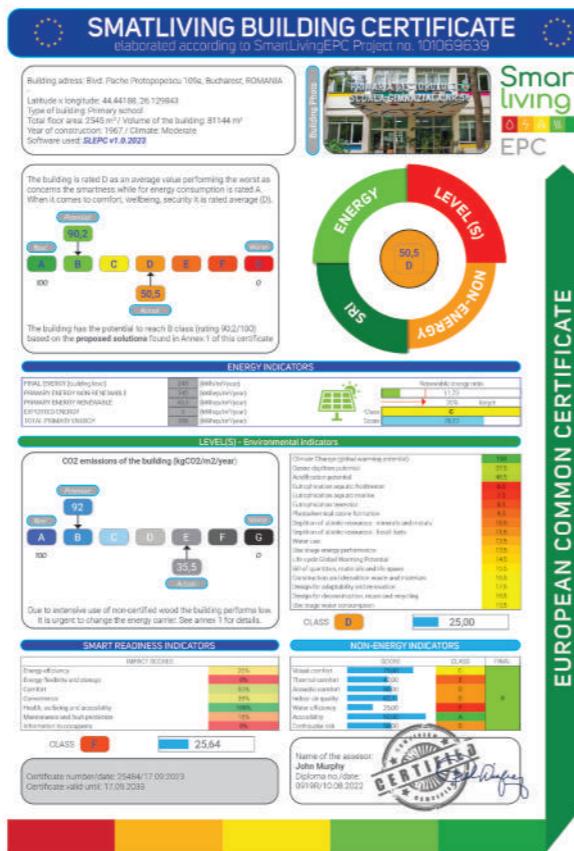
În conformitate cu prevederile legii 372/2005, republicată, cu modificările și completările ulterioare, facem și următoarele precizări foarte importante:

(1) certificatul de performanță energetică se elaborează în mod obligatoriu pentru apartamente, case, blocuri, clădiri de birouri, clădiri pentru învățământ, spitale, clădiri comerciale, clădiri pentru activități sportive, hoteluri și.a.m.d. care se construiesc, se vând, se închiriază sau sunt supuse renovărilor majore, pentru clădirile aflate în proprietatea/administrarea autorităților publice sau a instituțiilor care prestează servicii publice, precum și pentru clădirile cu o suprafață utilă totală de peste 250 m² ocupate de o autoritate publică și care este vizitată în mod frecvent de public;

(2) pentru clădirile sau unitățile de clădire care se vând sau se închiriază, investitorul/ proprietarul/ administratorul este obligat să pună la dispoziția potențialului cumpărător sau chiriaș, după caz, anterior perfectării contractului, o copie de pe certificat, astfel încât acesta să ia cunoștință despre performanța energetică a clădirii/unității de clădire pe care urmează să o cumpere/închirieze, după caz; contractele de vânzare-cumpărare încheiate fără respectarea prevederilor menționate aici, sunt supuse nulității relative, potrivit prevederilor Codului civil

(3) la încheierea contractului de vânzare-cumpărare, proprietarul are obligația de a transmite certificatul de performanță energetică, în original, nouui proprietar;

(4) la data înregistrării unui contract de vânzare-cumpărare imobil, respectiv de închiriere imobil,



proprietarul are obligația de a depune la organul fiscal competent o copie de pe certificat, iar originalul va rămâne în posesia proprietarului;

(5) certificatul de performanță energetică se elaborează și se eliberează de către auditorul energetic pentru clădiri, la solicitarea investitorului/proprietarului/administratorului clădirii/unității de clădire și este valabil 10 ani de la data eliberării înscrisă în certificat, cu excepția situației în care, pentru clădirea/unitatea de clădire la care există certificat în valabilitate, se efectuează lucrări de renovare majoră care modifică consumurile energetice ale acesteia;

(6) următoarele fapte constituie contravenții:

- nerrespectarea obligației auditorului energetic pentru clădiri de a înscrive în registrul propriu de evidență a activității a certificatelor de performanță energetică și a rapoartelor de audit energetic și se sancționează cu amendă de la 1.250 lei la 2.500 lei;
- nerrespectarea obligației auditorului energetic pentru clădiri și a expertului tehnic atestat de a transmite, în format electronic, editabil, la termenul stabilit prin lege, conținutul Certificatelor de performanță energetică și sintezele rapoartelor de audit energetic, și se sancționează cu amendă de la 1.250 lei la 2.500 lei;
- transmiterea de date și informații incomplete și/sau eronate în Certificatelor de performanță energetică și sintezele rapoartelor de audit energetic și se sancționează cu amendă de la 2.500 lei la 5.000 lei;
- nerrespectarea obligației de afișare a certificatului de către proprietarii/administratorii clădirilor de interes și de utilitate publică cu o suprafață utilă totală de peste 250 m², precum și la cele frecvent vizitate de public, și se sancționează cu amendă de la 1.250 lei la 2.500 lei;
- nerealizarea de către investitori a studiului privind fezabilitatea din punct de vedere tehnic, economic și al mediului înconjurător a utilizării sistemelor alternative de înaltă eficiență, și se sancționează cu amendă de la 2.500 lei la 5.000 lei;
- nerrespectarea de către investitorul/proprietarul/administratorul clădirii/unității de clădire, respectiv de către agenții imobiliari/agenții de publicitate imobiliară a informării potențialilor cumpărători sau chiriași, prin precizarea în anunțurile de vânzare sau închiriere a acestora informații din certificat privind indicatorii de performanță (clasa de performanță energetică, emisiile de CO₂, consumul de energie primară, consumul de energie din surse regenerabile etc.), și se sancționează cu amendă de la 1.250 lei la 2.500 lei
- emiterea certificatului de urbanism emis de către autoritățile administrației publice locale/județene competente, în vederea emiterii autorizației de construire, (i) fără a solicita pentru clădirile noi/ansamblurile de clădiri noi, întocmirea unui studiu privind fezabilitatea din punct de vedere tehnic, economic și al mediului înconjurător a utilizării sistemelor alternative de înaltă eficiență și (ii) fără a solicita încadrarea necesarului de energie al clădirilor în nivelurile NZEB prevăzute în Mc001-2022; acest certificat de urbanism se consideră incomplet, iar fapta constituie contravenție și se sancționează conform prevederilor art. 26 alin. (1) lit. h) și alin. (2) din Legea nr. 50/1991 privind autorizarea executării lucrărilor de construcții, republicată, cu modificările și completările ulterioare.

sistemelor alternative de înaltă eficiență, și se sancționează cu amendă de la 2.500 lei la 5.000 lei;



Ca urmare a precizărilor de mai sus, O.A.E.R., în calitate de co-autor al Mc001-2022 și de promotor cu responsabilitate al sustenabilității construcțiilor din România care generează mai mult de 30% din emisiile totale de gaze cu efect de seră, solicită:

1 - tuturor proiectanților și auditorilor energetici pentru clădiri să respecte reglementarea Mc001-2022 și legislația aferentă domeniului lor de activitate;

2 - tuturor reprezentanților serviciilor de urbanism din primării, să întocmească corect certificatele de urbanism, cu includerea prevederilor din legea 372 și din reglementarea tehnică Mc001-2022;

3 - Inspectoratului de Stat în Construcții să își exercite cu responsabilitate și consecvență rolul de autoritate de control, în baza procedurii PCC001/2013;

4 - tuturor notarilor publici să respecte întocmai prevederile legii 372 și să solicite la tranzacțiile imobiliare cu clădiri/unități de clădire/apartamente, certificatul de performanță energetică.

Experții O.A.E.R. stau la dispoziția tuturor celor interesați cu alte informații privind domeniul Performanței Energetice a Clădirilor.

office@oaer.ro

ORDINUL AUDITORILOR ENERGETICI DIN ROMÂNIA

OAEER membru afiliat IEQ-GA

O.A.E.R. (www.oaeer.ro) este o asociație profesională având ca obiectiv crearea cadrului organizatoric în vederea promovării măsurilor, concepțiilor și acțiunilor care să conducă la susținerea intereselor profesionale precum și la creșterea și perfecționarea activității absolvenților de învățământ superior de lungă durată și specialiștilor din cercetare, proiectare, execuție și exploatare, pentru realizarea unor clădiri perfor-

mante energetic. O.A.E.R. asigură totodată cadrul instituțional adecvat de manifestare a membrilor săi, reprezentând și ocrotind interesele auditorilor energetici pentru clădiri. O.A.E.R. a făcut parte din consorțiul condus de Universitatea Tehnică de Construcții București (U.T.C.B., www.utcb.ro) pentru elaborarea Mc001/2022, alături de Asociația Inginerilor de Instalații din România (A.I.I.R., www.aiiro.ro).

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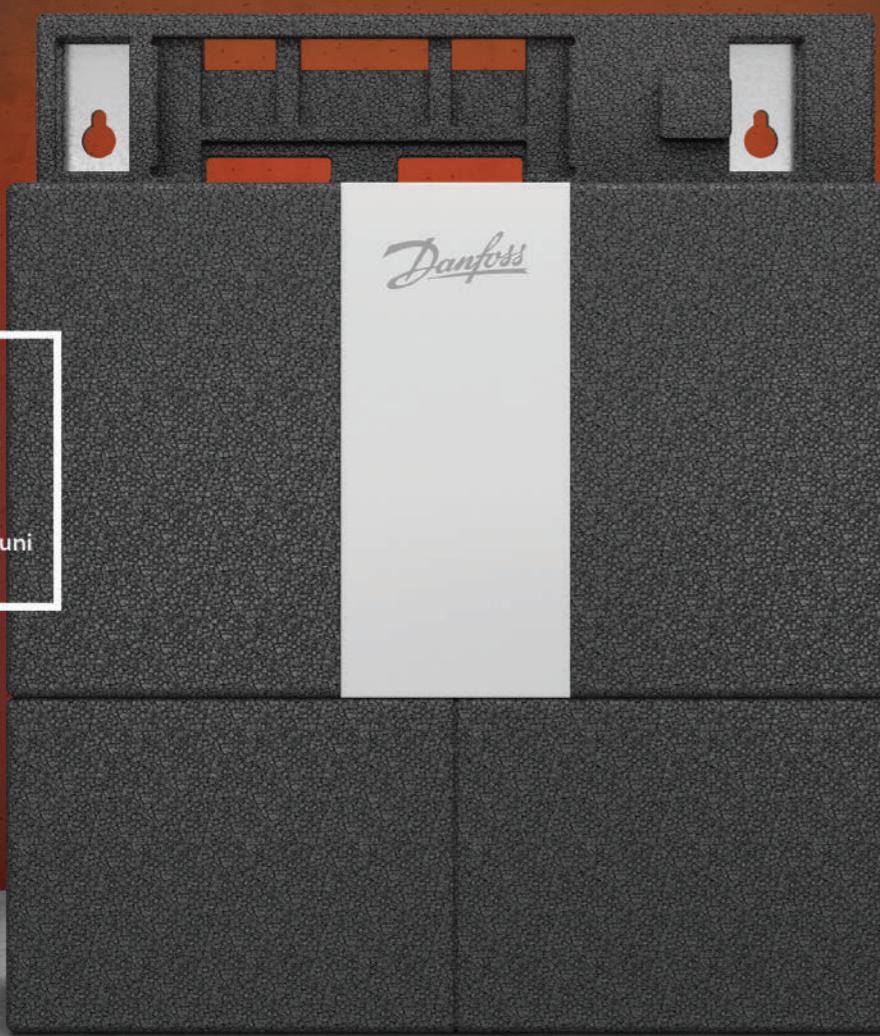
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Proiectele de încălzire rezidențială pun accentul pe timp, bani și fiabilitate. Din acest motiv, inginerii noștri au reproiectat complet modulele de apartament EvoFlat. Au folosit cele mai inovatoare tehnologii disponibile la ora actuală pentru a proiecta modulul de apartament al deceniului următor. Rezultatul: EvoFlat 4.0.

Noul EvoFlat 4.0 este:

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- prevăzut cu componente de cea mai înaltă calitate pentru o durată de viață mare
- extrem de eficient din punct de vedere energetic pentru a reduce la minimum costurile de încălzire
- cel mai ușor modul de apartament de pe piață pentru a facilita instalarea rapidă



Mai bun. Succesul este asigurat de noul „corp” inovator din interiorul modulului. Este realizat din compozit din PPS ranforșat cu fibre de sticlă. Compozitul este puternic, asigură emisii de căldură limitate, are o suprafață netedă care evită depunerile de calcar și infundarea și este foarte ușoară. Este inovația perfectă care elimină conductele, cuplările și vanele tradiționale din alamă sau oțel inoxidabil întâlnite în majoritatea modulelor. În plus, acest modul este conform cu viitoarele reglementări RoHS din 2024.

Mai ușor. „Corpul” din compozit special include și componente hidraulice. De la componente tradiționale, cum ar fi regulatorul de presiune diferențială, bypassul de vară și regulatoarele de temperatură, corpurile de vană din alamă sunt acum integrate în „corpul” din compozit. Acest lucru reduce semnificativ greutatea și utilizarea materialelor.

Mai simplu. Toate componentele rămase sunt montate pe „corp” cu ajutorul racordurilor cu noul design de fixare cu cleclic. Fiecare componentă poate fi accesată cu ușurință din partea frontală. Acest lucru ușurează lucrările de service sau de modernizare. Pentru a facilita înlocuirea, noul EvoFlat 4.0 are aceleași racorduri și distanțe între elemente ca și modulul EvoFlat actual.

EvoFlat 4.0:

- Modul de apartament compact pentru încălzire directă și/sau apă caldă menajeră
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Interior Environmental Simulation and Economic Evaluation for Energy Upgrades in a Church

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Abstract

Background: Our study aimed to determine the most efficient heating system for a 16th-century Romanian heritage church. We compared the existing mixed system (static heaters and hot air heating) with underfloor heating, using computational fluid dynamics (CFD) for indoor climate analysis. Two turbulence models, $k-\varepsilon$ and $k-w$, aided our research. Results indicated that underfloor heating produced lower temperatures but had higher air velocities, particularly under the towers zone, when compared to the existing system. In conclusion, the underfloor heating not only provided better thermal comfort for churchgoers but also ensured the preservation of the heritage structure.

Keywords: indoor climate; energetic rehabilitation; church heating; CFD modelling

1. Introduction

Buildings play a pivotal role in the European Union's energy efficiency strategies. In Romania, heating accounts for 45% of a building's total energy consumption, highlighting the need for enhanced energy efficiency. Especially significant are heritage sites like painted churches, renowned for their frescoes that contribute to both national and global heritage.

The importance of preserving these interior artworks aligns with the mandates of the European Directive 31/2020/EU.

Romanian churches are not just places of worship; they represent a legacy intertwined with the country's history and culture. Originating from Christian

rituals, these churches were built to honor the divine. Over centuries, advances in construction techniques, the use of robust materials, artistic endeavors in the form of frescoes, and the incorporation of heating systems have transformed these edifices, enhancing their longevity and comfort.

Heritage buildings, particularly churches and monastic settlements, have significant tourism potential. Their inclusion in popular tourist circuits has led to a surge in visitors. While these visitors contribute to the ambiance during religious ceremonies, they also influence the church's internal microclimate.

Moreover, as efforts intensify to modernize these structures to provide thermal comfort during colder months, the influx of tourists grows. However, these changes can have unintended consequences.

Modernization can disrupt the building's indoor climate, leading to issues like condensation in areas with pronounced thermal bridges, such as wall intersections, the base, and the roof. The balance between preserving heritage, ensuring comfort, and accommodating tourists is delicate and demands thoughtful consideration.

Historical buildings, which include museums, schools, offices, hospitals, and hotels, operate for numerous hours yearly, emphasizing the need for energy efficiency. In cities like Jassy, notable buildings like the St. Three Hierarchs Monastery Assembly and the Palace of Culture are landmarks. Churches present unique energy challenges due to their sporadic use and the distinct thermal comfort requirements of their attendees.

Although energy efficiency certificates aren't mandated for heritage sites, they're recommended to understand a building's insulation and energy needs. The goal of rehabilitating and modernizing these structures is to enhance their energy efficiency, affecting heating, water heating, and lighting. Studies, such as one conducted in Austria on cult buildings, revealed that those with high thermal mass exhibited consistent interior microclimates, with stable temperatures and humidity levels throughout seasons.

Such studies provide a foundation for assessing indoor climate strategies, especially considering the similarities between Austrian and Romanian climates. Importantly, heating system parameters significantly impact indoor climates.

In some situations, balancing factors like external weather, visitor comfort, and heritage conservation can be challenging. Moreover, inadequate insulation in over 30% of churches has led to issues like mold and condensation, particularly around thermal bridges.

The overarching benefit of increasing energy efficiency is the positive environmental impact. However, solutions aimed at modernizing heating and lighting should not compromise the aesthetic and historical integrity of the buildings.

While previous research primarily focused on evaluating indoor climates of existing heating systems, this study's objective is to contrast the energy consumption of the current and proposed heating systems in a Romanian church, aiming to pinpoint the optimal heating solution.

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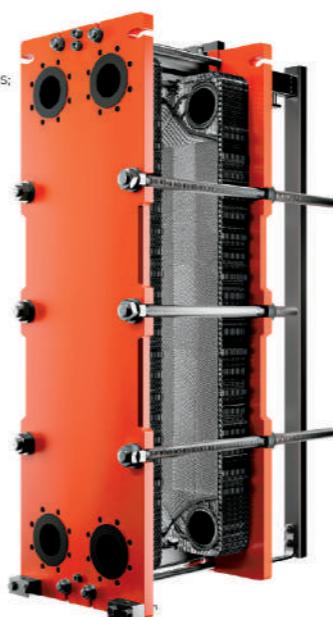
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Fig.1. (a) Degradation due to the appearance of condensation at the base. (b) Degradation captured in images with thermal vision cameras show the areas with thermal bridges that favor the appearance of condensation

2. Materials and Methods

We examined the heating system of a 16th-century orthodox church in Jassy, dedicated to the Three Holy Hierarchs. Located in Romania's third wind and climatic zones, the church faces winter temperatures of -18°C. Currently using a mixed heating system (static heaters and hot air heating), we compared

its efficiency with an underfloor heating system. The church, shaped like a Greek cross, consists of a narthex, nave, and altar. Having undergone restorations due to fires and earthquakes, it exhibits Moldavian architectural features with Transylvanian gothic influences.

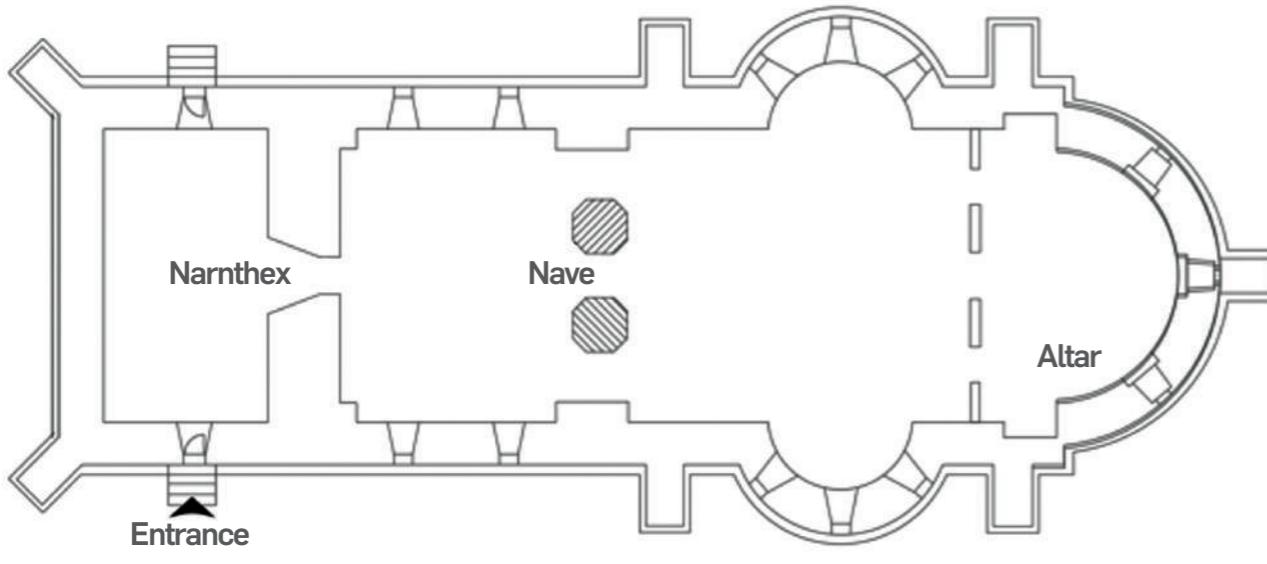


Fig.2. The current form in the church plan of Three Holy Hierarchs in Jassy

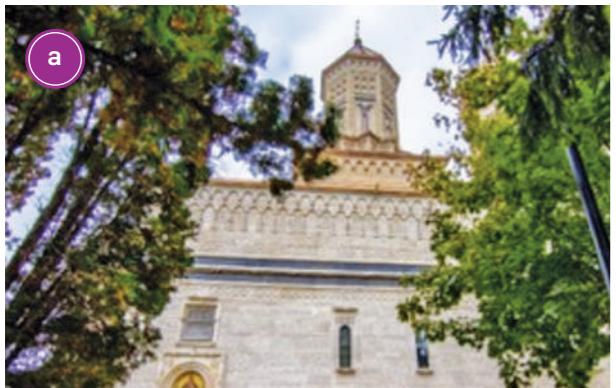


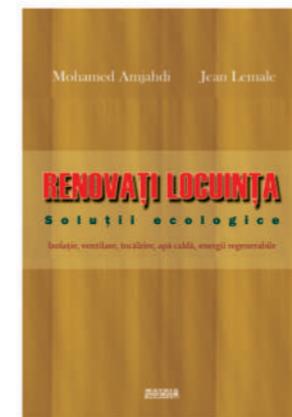
Fig.3. View of the Three Holy Hierarchs church in Jassy: (a) main entrance and (b) side view

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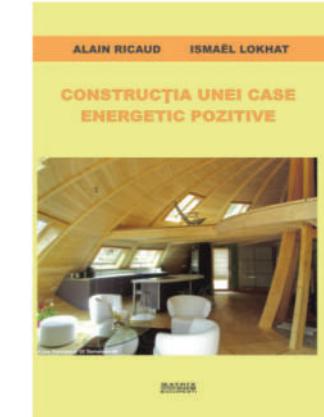
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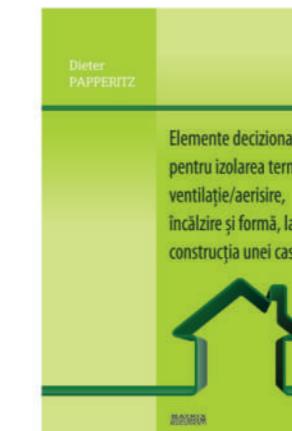
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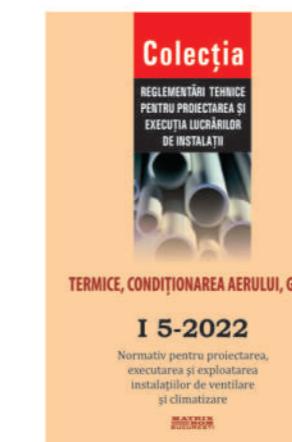
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The interior microclimate from the church, as well as of the physical parameters, could not be determined without investigative tools. For the microclimate in the church, we

used sensors from Testo that were mounted in the church during the winter for 2 months. The sensors were placed in the area of the second tower of the church, in a vertical plane.

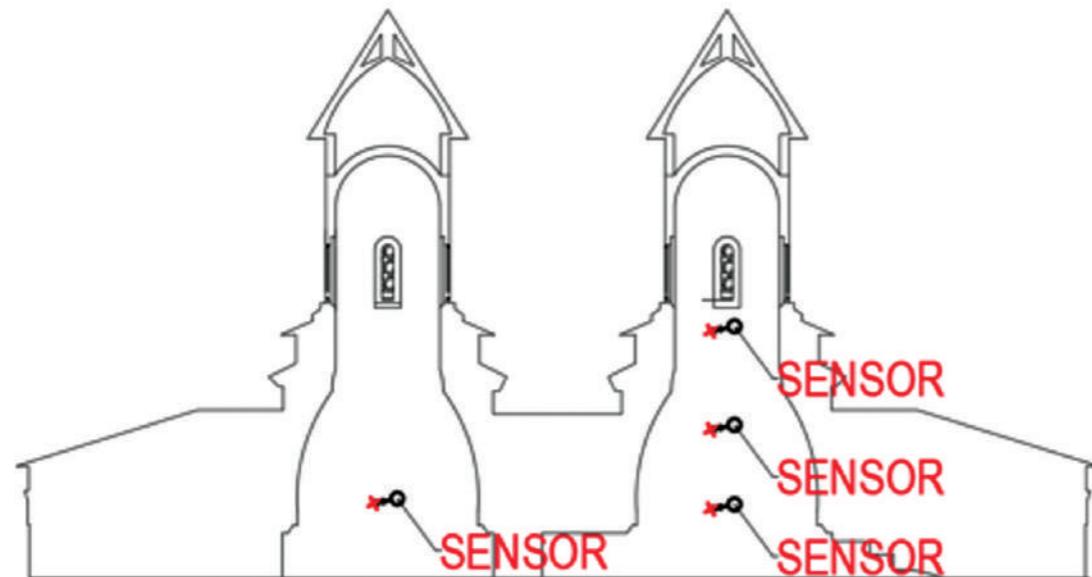


Fig.4. Sensors placed in the church

We utilized thermal imaging in construction to assess heat loss, insulation defects, air infiltration, and areas prone to dampness and mold. This technology also enabled us to study material defects and monitor heating systems for temperature fluctuations. Using equipment, we recorded temperature, humidity, and air velocities with sensors placed 1.8 meters

high, away from drafts, cold radiation, and direct heating equipment influence. In 2017, we analyzed the church's mixed heating system. Measuring both indoor and outdoor winter temperatures, and considering building envelope parameters, we created a computational fluid dynamics (CFD) model to evaluate hidden effects on the paints and walls.

Table 1. The boundary conditions imposed for the computation fluid dynamics (CFD) analysis in the Three Hierarchs church.

No.	Envelope element	Type of the heating system	
I	II	III	IV
Temperature (°C)		Static heaters with hot air system	Underfloor Heating System
Exterior Walls		-16	-16
Ceiling		-15	-15
Input grids for hot air		35	-
Ground plate		10	10
Windows and Doors		-16	-16
Pressure (Pa)	Relative pressure		
Heat transfer coefficient U (W/m²K)	Exterior walls	0.652	0.652
	Windows and doors	2.379	2.379
	Ceiling	1.518	1.518
	Ground plate	0.818	0.818
	Tower walls	1.276	1.276
Air velocity(m/s)	Inlet grids for hot air	0.25	-
	Extraction grids	0.15	-
Heat flux (W/m²)	Static heater	200	-
	Underfloor heating	-	100
Heat flow generated by people is imposed at 80 (W)			

The limit conditions imposed for the inlet air temperature and air velocity were taken from the operating regime of the heating installation, and the heat flux

imposed on the radiators was determined from a guide for determining the thermally equivalent surface of a heating body.

$$Q = \dot{m} \times C_p \times \Delta T \quad (1)$$

where:

\dot{m} – fluid flow rate;
 C_p – specific heat of the fluid;
 ΔT – the temperature difference between supply pipes lines and return pipes lines from boilers.

We chose $k-\epsilon$ and $k-\omega$ turbulence models for the church's CFD analysis based on literature. Starting with 2 million unstructured meshing elements, we increased to 8 million for the existing heating and 10 million for the proposed system, observing no parameter variations. Using the Friendly-Heating Project and Climate for Culture studies, we then conducted simulations.

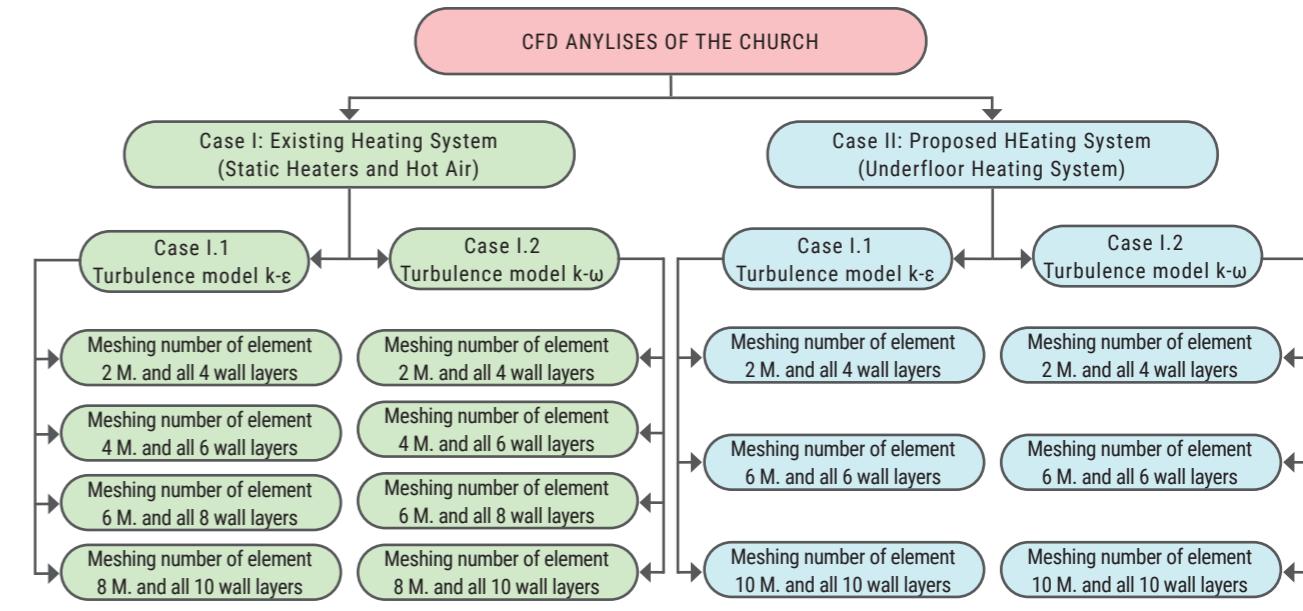


Fig.5. CFD analysis scheme of the church. We evaluated the existing heating system and the proposed one; for each of these, we used two different turbulence models ($k-\epsilon$ and $k-\omega$). We used different levels of meshing and wall layers that were gradually increased until we did not have any variations in the studied parameters.

3. Results

3.1. Thermovision Images

The monument, a part of Romania's cultural heritage, represents the area's architectural style and is over 350 years old. Built from brick masonry, weather and time have degraded its structure. High heat losses have caused condensation,

affecting finishes and leading to detaching paintings and plasters. Air currents from heating further dry and detach wall paints, and wall thickness differences cause heat losses, leading to damaging condensation and mold.

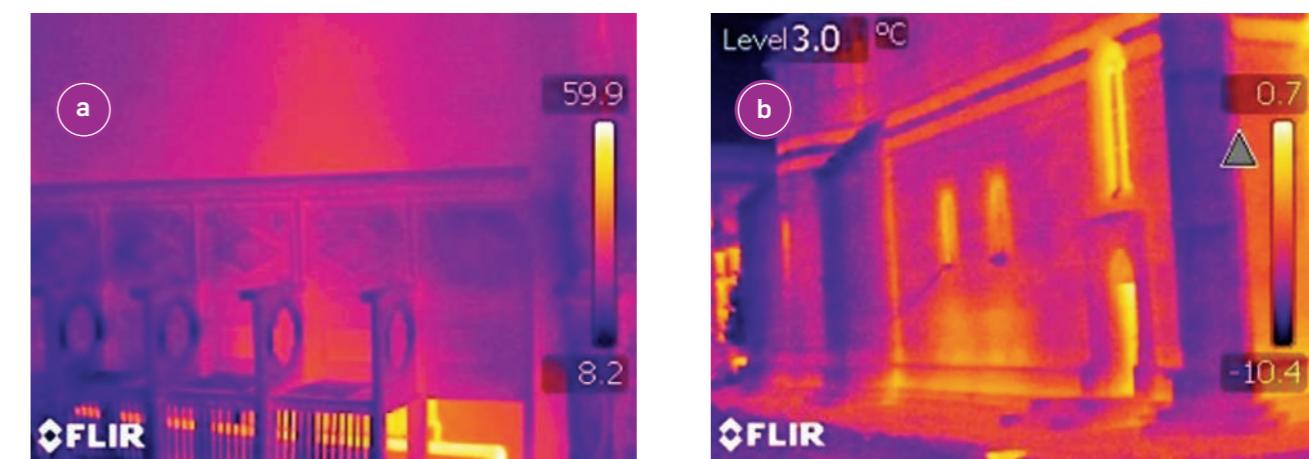


Fig.6. Thermal vision images that capture (a) the effects of the static heater over the walls and (b) thermal bridges in the outer walls.

The historical church features a non-insulated roof, metallic windows, and marble flooring. Walls vary from 80-180 cm thick. The church spans 351.47 m²

with a volume of 2710 m³. It uses electricity and thermal systems, with incandescent lighting and radiator heating.

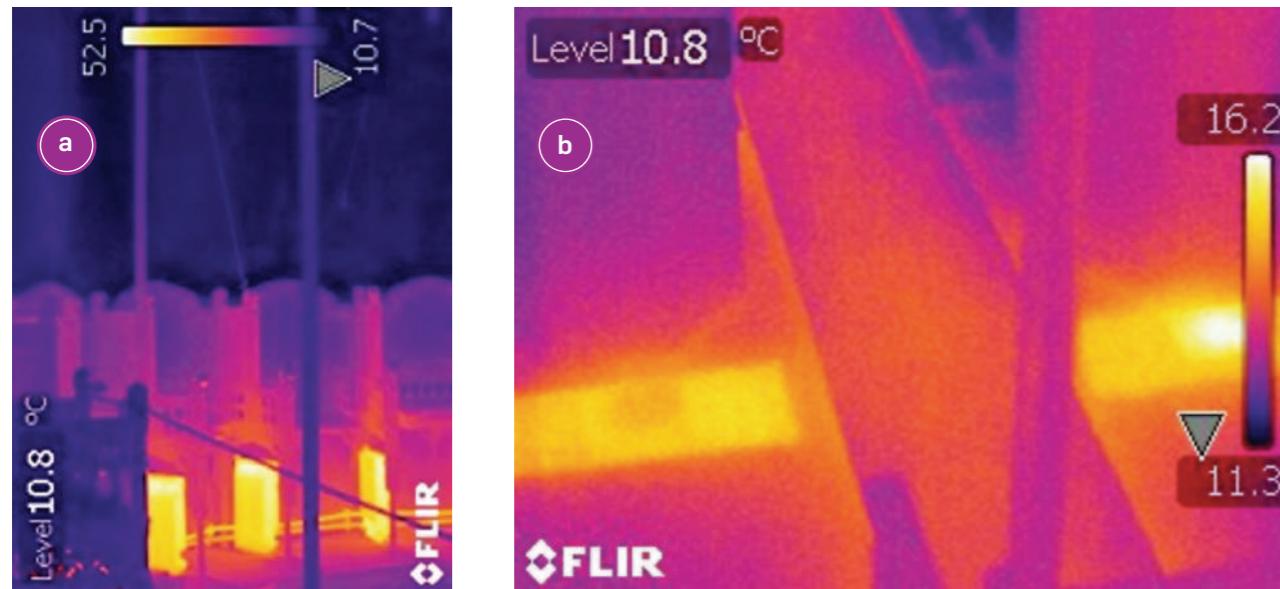


Fig.7. Thermal imaging camera images of the heating system in the church

3.2. Heating with Radiators Modelled with Ansys Fluent

The primary goal of the CFD analysis on the church's existing heating system was to comprehend its impact on the church's indoor environment, focusing on the envelope elements and thermal comfort of attendees. This study aimed to offer solutions to observed church degradations using both direct observations and thermal imaging. These solutions target enhancing indoor climate, preserving the church's heritage, and ensuring worshipper comfort.

For the CFD modelling, ANSYS FLUENT software was employed for a 3D study of the indoor environment. A finely detailed mesh with steps ranging from 5 cm to 8 cm was generated, utilizing a Cartesian coordinate

system. Standard, simple equations derived from the first order were used to solve flow, continuity, and energy aspects. Natural circulation from radiators introduced the heat, not forced ventilation, leading to the choice of the standard k-ε model and Boussinesq's approximation for air density.

Figure 8 illustrates the air velocities with varying temperatures and their interactions within the church's architecture. The results show that warm air rises, forming a layer at the top, while cooler air settles at the bottom. This movement leads to a noticeable stratification of air temperatures inside the church.

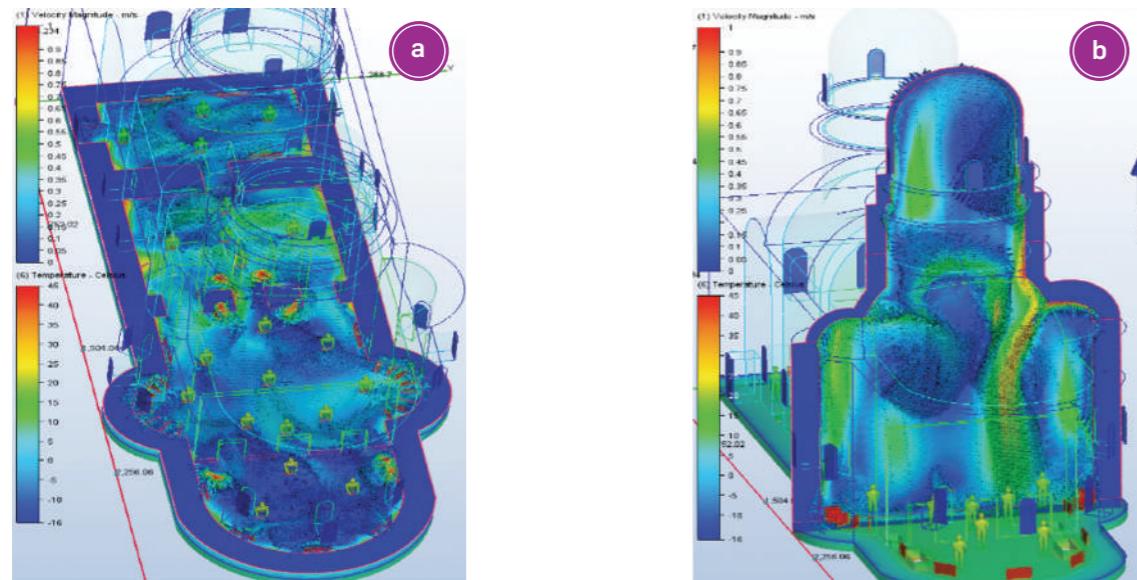


Fig.8. Profiles of temperature and air velocity contour in the church after CFD modelling: (a) horizontal velocity field in the occupied area and (b) vertical velocity field of air currents in the area of the nave

The rising air around radiators adversely affects wall paintings by lifting dust particles onto them, as illustrated in Figure 8. Using two turbulence models and in situ measurements, a statistical boxplot

analysis was conducted to process and present the data efficiently. Analyzing air currents revealed variations, with higher values in the nave. Figure 9 depicts outcomes for the proposed heating system.

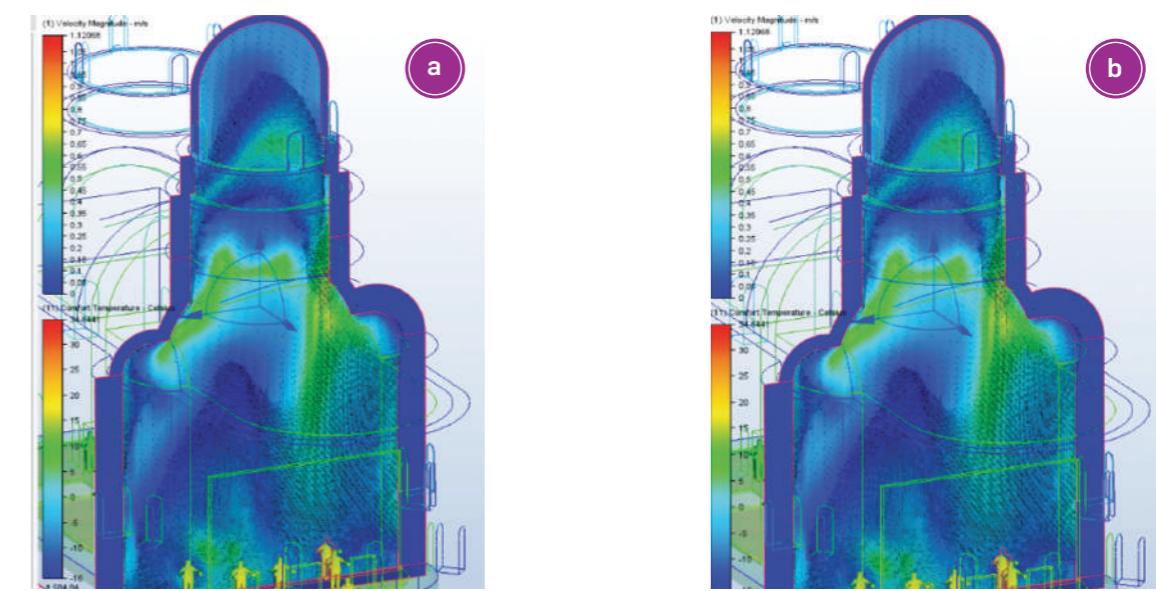


Fig.9. Profiles of temperature and air velocity contour in the church after CFD modelling: (a) vertical velocity field of air currents in the area of the nave and (b) horizontal velocity field in the Boxplot graphs comparison showed underfloor heating had the lowest temperatures

Air velocities with this system were notably higher in the nave area. The k-ε turbulence model's values

aligned more closely with the indoor air quality (IAQ) sensor measurements.longitudinal section.

Comparison between temperature values from simulation and in situ measures

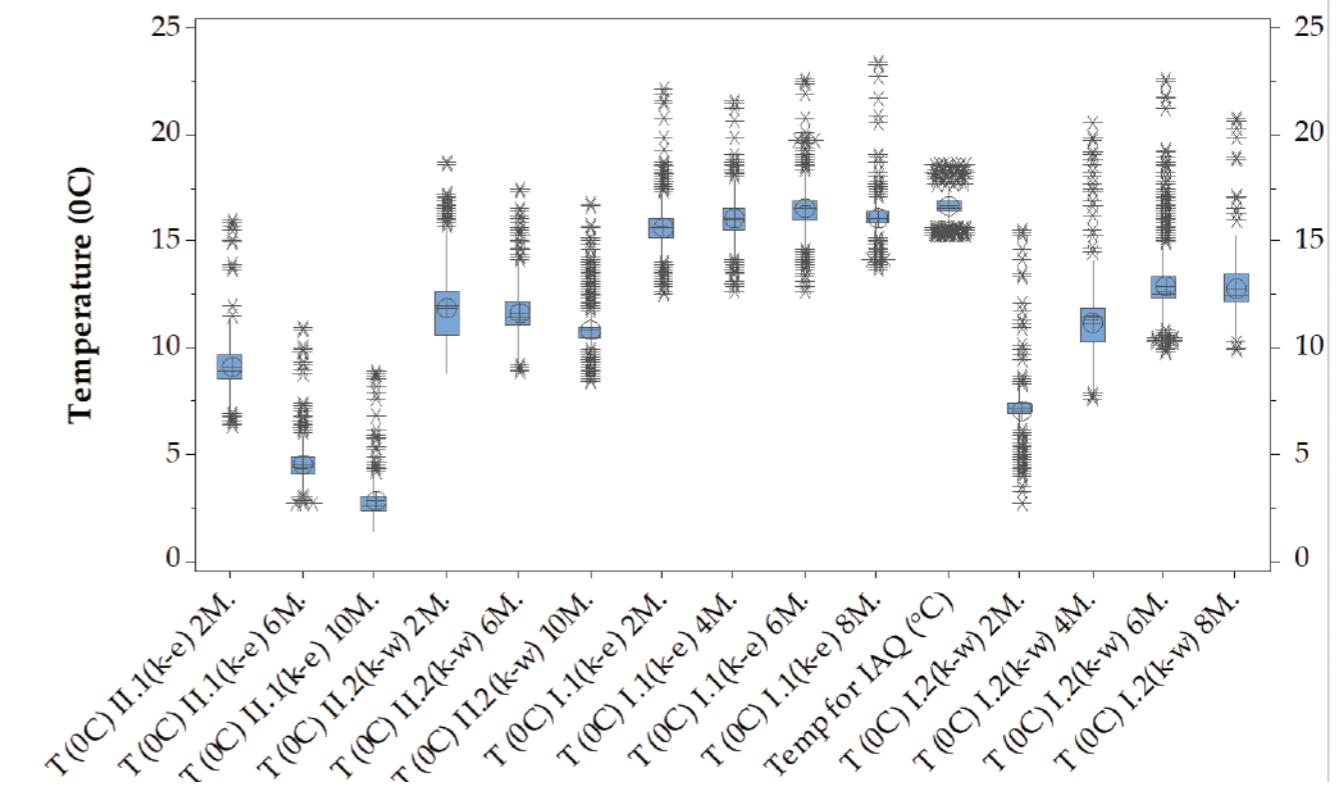


Fig.10. Comparison between temperature values for both turbulence models (standard k-ε and k-ω): the existing heating system, the proposed heating system, and the indoor air quality (IAQ) probe

Comparison between air velocity values from simulation and in situ measures

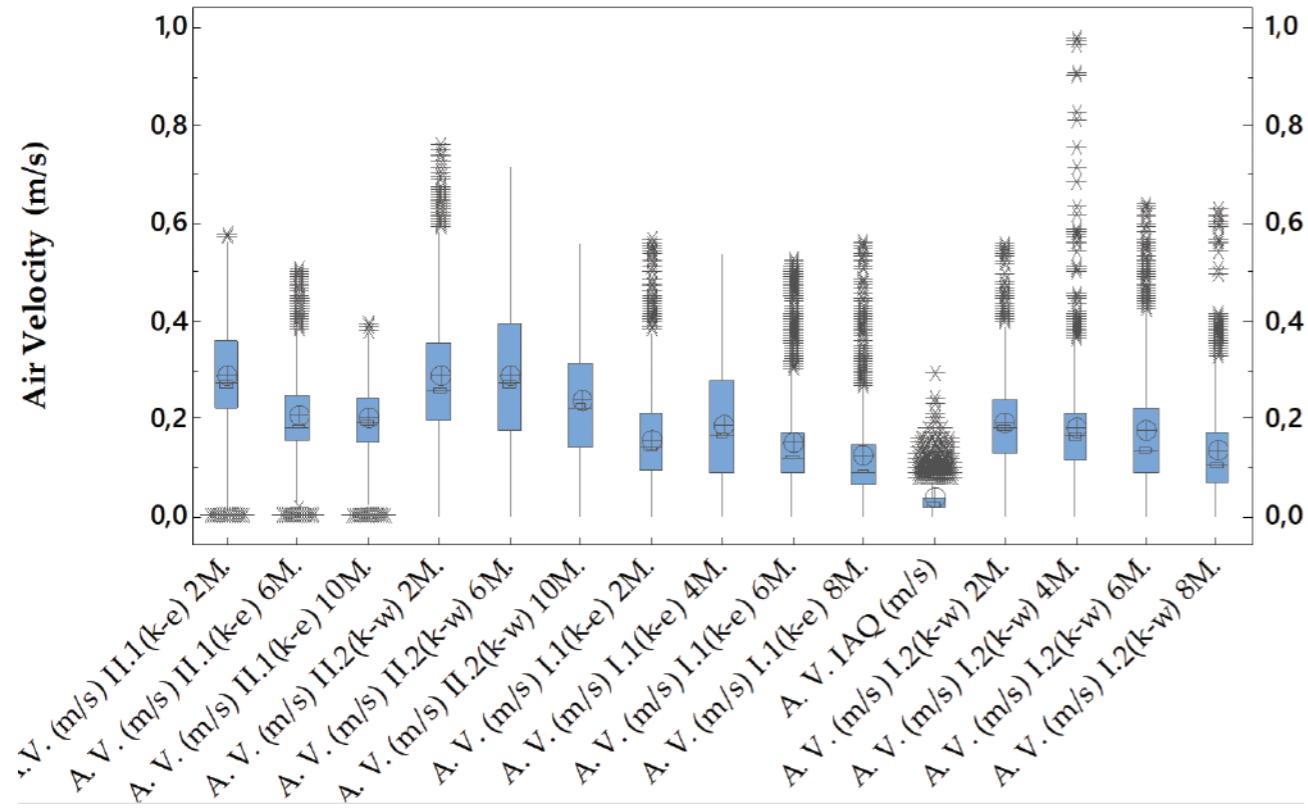


Fig.11. Comparison between air velocity values for both turbulence models (standard $k-\epsilon$ and $k-\omega$): the existing heating system, the proposed heating system, and the indoor IAQ probe

3.3. Analysis of the Studied Building Energy Performance

We also performed a thermo-technical calculation of the envelope elements according to the normative C107-2005. We determined the corrected thermal resistances of the closing elements R' ($\text{m}^2\text{K}/\text{W}$) com-

pared to the standard thermal resistances R'_{\min} ($\text{m}^2\text{K}/\text{W}$). The criterion for satisfying the requirement of thermal insulation was $R' \geq R'_{\min}$. The comparative values are presented in Table 2.

Table 2. The thermomechanical characteristics of the existing envelope

Elements	A	R'	R'_{\min}
	m^2	$\text{m}^2\text{K}/\text{W}$	$\text{m}^2\text{K}/\text{W}$
North wall	147.16	0.652	1.800
West wall	51.68	0.652	1.800
East wall	61.41	0.652	1.800
South wall	147.16	0.652	1.800
Roof	305.91	1.518	5.000
Decking	266.01	0.818	4.500
Windows	35.36	0.330	0.770

The analysis showed that most of the building envelope elements did not meet the minimum thermal insulation requirements. The annual consumptions were calculated according to the normative NP 048-2000. This norm takes the heat transfer in a non-stationary regime through a building envelope

into account. The heat contributions due to the human activities and the solar radiation were also considered. The estimation of annual consumptions was used for the energy certificate.

In this way, the annual consumption was as follows:

Yearly consumption for heating:

$$Q_{\text{heat}}^{\text{year}} = 257,35 \text{ kWh/m}^2\text{year},$$

Yearly consumption for hot water preparation:

$$Q_{\text{hotwater}}^{\text{year}} = 30,15 \text{ kWh/m}^2\text{year},$$

Yearly consumption for lighting preparation:

$$W_{\text{lighting}}^{\text{year}} = 28.76 \text{ Wh/m}^2\text{year},$$

Total annual consumption:

$$Q_{\text{heat}}^{\text{year}} = 316.26 \text{ kWh/m}^2\text{year}.$$

3.4. Completion of the Energy Certificate

Churches have intrinsic value via their heritage, and they also have energy consumption, especially in a climatic zone where the duration of the heating season lasts for several months. In Romania, the duration of the heating season is, on average, 3600 degrees-days (K·h).

This is the reason why we considered it necessary to carry out an energetic classification of the church that we analyzed.

The energy certificate of the building was decided based on its consumptions, and it was attributed the energy classification "D" and a value of Q (Heating/Year) = 3162 kWh/m² for the annual consumption of heat for heating, hot water, and lighting (Figure 12).

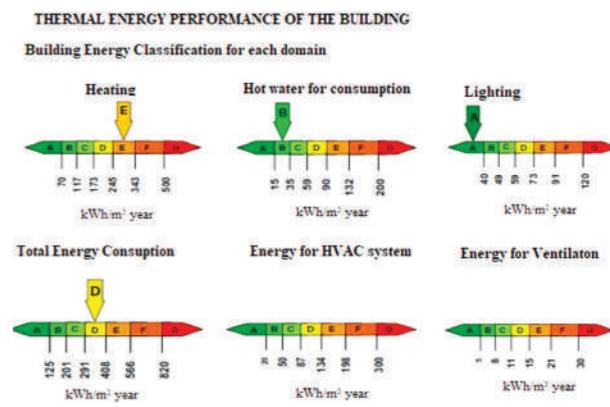


Fig.12. Grids regarding the energy classification of the audited building kWh/m² year

3.5. Proposals on Energy Modernization Solutions

The church's historical facade restricts adding thermal resistance, but improvements can be made to the floor and roof. Two rehabilitation models were proposed:

Thermal Rehabilitation:

- A 15 cm mineral wool layer was suggested for the floor under the bridge, yielding a corrected thermal resistance of $R' = 3367 \text{ (m}^2\text{K/W)}$.
- the ground floor, giving a corrected resistance of $R' = 3138 \text{ (m}^2\text{K/W)}$.

Operational Efficiency and Thermal Rehabilitation:

- Efficient static heaters, adjusted for the thermal rehabilitation solutions.
- Thermostatically regulated valves on static heaters.
- Automation of thermo-energetic equipment.
- Water-efficient sanitary fittings for domestic hot water.

- Exploration of modern, renewable energy-based equipment for hot water preparation.

For lighting energy conservation:

- Complete restoration of lighting installations.
- Appropriate number of luminaires based on room use and required illumination levels. Preference for luminaires with fluorescent lamps or LEDs with capacitors and electronic ballasts for high luminous efficiency.

Through thermal rehabilitation, the building's insulation improved, raising its energy certificate rating.

Combined with indoor services upgrades, the building achieved a "B" energy classification with an annual consumption of 151.19 kWh/m²year for heating, hot water, and lighting. The reference building had separate energy classifications for thermal utilities.

3.6. Economic Aspects Regarding the Two Modernization Packages

The economic analysis was a simplified form of assessing the amortization of investments. (Tables 3 and 4). This analysis was based on the following assumptions and values:

- at the date when the energy audit was performed, the average cost of the thermal energy was 55.16 Euro/Gcal, equivalent to 0.12 Euro/kWh [7], in which:
- Gcal - gigacalories.

The (simple) duration of the investment recovery, N_R (years):

$$N_R = C_{\text{INV}} / (\Delta E \times c_{\text{et/ee}}) \quad (2)$$

in which:

C_{INV} —the cost of energy modernization works (Euro).
 ΔE —energy savings achieved by applying energy

modernization solutions (kWh/year).
 $c_{\text{et/ee}}$ —the specific cost of heat/electricity, (Euro/kWh);

The average cost of thermal energy when the energy audit was performed, was:
 $c_{\text{et}} = 0.12 \text{ Euro/kWh}$

The average cost of electricity when the energy audit was performed, was: $c_{\text{ee}} = 0.1 \text{ Euro/kWh}$.
 e —the cost of the energy unit saved during the life of the solution (Euro/kWh):

$$e = C_{\text{INV}} / (\Delta T \times N_S) \quad (3)$$

in which:

N_S —the estimated lifetime of the energy upgrade solution = 15 years .

Table 3. Individual consumption per consumption grid and total annual consumption in (kWh/year) for each type of proposed solution.

Modernization Package	Heating consumption	Domestic hot water consumption	Consumption of electrical installation	Total consumption of the source
	kWh/year	kWh/year	kWh/year	kWh/year
Construction	70516	10598	10109	91223
Constructions and plumbing	43221	2552	7365	53138

Table 4. Comparison of the proposed solutions

Modernization Package	Energy-saving	Lifespan Ns	Investment cost	Duration of recovery NR	The cost of energy saved E
	kWh/year	years	Euro	years	Euro/kWh
Construction	19933	30	40256	13.46	0.0673
Constructions and plumbing	58018	20	43623	9.40	0.0376

4. Discussion

The study evaluated different heating systems in churches and the implications on architectural heritage. Of all systems, underfloor heating had the lowest temperatures but the highest air velocities, notably in the nave. The k-ε turbulence model produced temperature and air velocity values most similar to those measured with IAQ sensors. This is the inaugural study that has assessed these turbulence models for church heating systems and authenticated the k-ε model against IAQ sensors.

The energy makeover upgraded the church's energy classification from class D to B. Issues identified included air circulation causing rapid drying of artworks

and artifacts, dust circulation and deposition in cold areas, and condensation issues related to radiator heating. Historically, heating designs aimed for cost-efficiency, often neglecting internal climate quality.

Modern-day considerations strive for occupant comfort. "Climate for Culture," a European project (2009–2014), assessed climate impacts on heritage buildings, forecasting up to 2100 using the REMO model. The European Friendly-Heating Project (2009–2014) also explored heating and conservation in heritage sites. The study underscores the importance of evaluating heating systems for both comfort and preservation of churches' architecture and artifacts.

5. Conclusions

In conclusion, our study highlighted that there is a continuous interaction between the parameters of the indoor climate and heritage conservation. Thus, we noticed that the temperature, humidity, and velocity of the air currents influenced the state of conservation of the existing heritage inside the churches, and the k-ε turbulence model had

temperature and air velocity values closer to those measured with IAQ sensors.

In our study, the underfloor heating system was more efficient than the existing heating system (static heaters and hot air heating), ensuring heritage conservation and high thermal comfort to churchgoers.

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During the Supporters Committee, Energate will hold an Expert Talk on "Energate standardisation on financing energy efficiency, HVAC as a Service, EU taxonomy".

The Committee Meetings are open to REHVA Members and Supporters only (except for the Supporters Committee - attendance of the Energate Expert Talk is open to all).

The first day will end with a REHVA Dinner at the Thon Hotel.

This event is free of charge; however, registration is mandatory. Please take note that cancellation is also required.

Day 2: Policy Conference (14th November)

The second day of the Summit will feature the yearly Policy Conference. All policy instruments enabling and facilitating the clean energy transition in the building sector are falling into place in 2023 at EU level with the adoption of the Energy Efficiency Directive (EED), the Renewable Energy Directive (RED) and the Energy Performance of Buildings Directive (EPBD) as core elements of the 'fit for 55' package (designed to realise the EU Green Deal and more recently also REPowerEU).

The journey to bring the buildings related EU policy instruments to practice on the ground doesn't end here. The EU's Member States (MSs) need to adequately transpose, implement, enforce and monitor them while fostering and ensuring their practical application by skilled building professionals.

Furthermore 2023 is the **European Year of Skills**, meant to promote upskilling and reskilling opportunities and EU funding possibilities, to support take-up, implementation and delivery on the ground. Without any coincidence, the EU Green Deal Industrial Plan presented in February 2023 has as third pillar "enhancing skills", at all levels and for all people, with inclusiveness of women and youth at the heart of the Plan.

Against this backdrop the session organizers, targeting foremost policy makers and at large the building sector stakeholders, drawn together some of the key institutional, professional and business actors to foster EU-national coordination, at the fastest pace possible, for bridging the gap 'available-needed' professionals, with an emphasis also on Indoor Environmental Quality (IEQ) and Digitalisation:

- Policy and financing instruments as linchpin for the skills framework.
- Education, training, upskilling and reskilling.
- Best practices for designing effective training programmes.

The timing is nothing short of ideal for the EU level professional associations and their national member associations to step up and play a twofold game changing role for EU-national coordination:

- Support the adequate transposition of the EED, RED and EPBD in the EU's MSs while also future proofing the feasibility for practical implementation within the specific national contexts.
- Bridge the skilled building professionals' gap in collaboration with the national authorities, financing institutions and all concerned stakeholders of the building sector.

The day will end with a session held by MODERATE: Workshop with building professionals & EPB Expert.

Fees might apply if you fail to cancel your registration at least 5 days prior to the conference. For any questions or cancellation requests, email info(at)rehva.eu.



Exploring The Potential Of Adaptive Buildings Systems To Users' Need And Building Occupant Interaction (Summary)

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Abstract

Adaptive-Comfort-Control-Implemented Model (ACCIM), which uses indoor temperature to determine comfort levels, extends the adaptive comfort models beyond naturally ventilated spaces. Personalized ventilation and comfort systems, influenced by occupant's feedback and real-time sensations, are proposed for a more energy-efficient and occupant-focused building.

Advanced PCS and models predicting user behavior, as well as local comfort models, are considered for more nuanced and personalized control of indoor climates. These suggest a significant potential for energy conservation and improved thermal satisfaction in building design and operation, prompting further research in this transformative area.

Keywords: Adaptive thermal comfort; Energy efficiency; Climate change; Adaptive setpoint temperatures; Local comfort model



Introduction

Inside the buildings, the only thing that has not changed in more than 100 years is the control of the indoor environment in mechanically conditioned buildings, where strict temperature setpoints are implemented.

These strict temperature setpoints are responsible for part of that 30% of global CO₂ emissions ascribed to the building sector and a high level of thermal dissatisfaction among office users. In fact, if the setpoint dead-band – range of temperatures between heating and cooling setpoint where it is not necessary to intervene with HVAC, except for hygienic air changing rate – is broadened even just by 1°C, the annual HVAC energy use for heating and cooling is reduced by approximately 10%, and this increase of variability for indoor conditions is verifiably desired by human beings.

The actual paradigm of a one-size-fits-all (one set-point temperature that should satisfy all occupants), used to control modern buildings with centralized mechanical systems is flawed. Diversity in thermal preferences underscores the need for a personal approach.

Even while the junction of thermal comfort modeling and building control may appear obvious, there are still significant difficulties in doing so. "Occupant centric" control techniques are hardly informed by occupant feedback because they are typically trained using building data.

While occupant data is used to generate thermal comfort models, these models are rarely incorporated into building controls. It is crucial that the communities of building control and thermal comfort work together across disciplines. Reducing the energy consumption of buildings is the driving force behind the advancement of control algorithms for HVAC (heating, ventilation, and air conditioning) systems.

Research on data-driven techniques like deep learning has been stimulated as a result. The only occupant data employed in these "occupant-centric" approaches, aside from whether the room is empty or not and probabilistic occupancy patterns, is building data that is used to train their controllers.

The development of data-driven models has encouraged researchers in the field of thermal comfort to examine the advantages of using physiological, environmental, and personal variables to predict thermal comfort. Our team has work in the past on innovative concepts such as personalized ventilation, adaptive thermal comfort theory and development of a comfort equation for Romania, local thermal comfort theory using a physiology-based approach, biometric correlations between the metabolic parameters and the human breathing flows.

All our developed knowledge and the existing literature, allow us to propose several topics to be advanced at the scale of the smart buildings of the future:

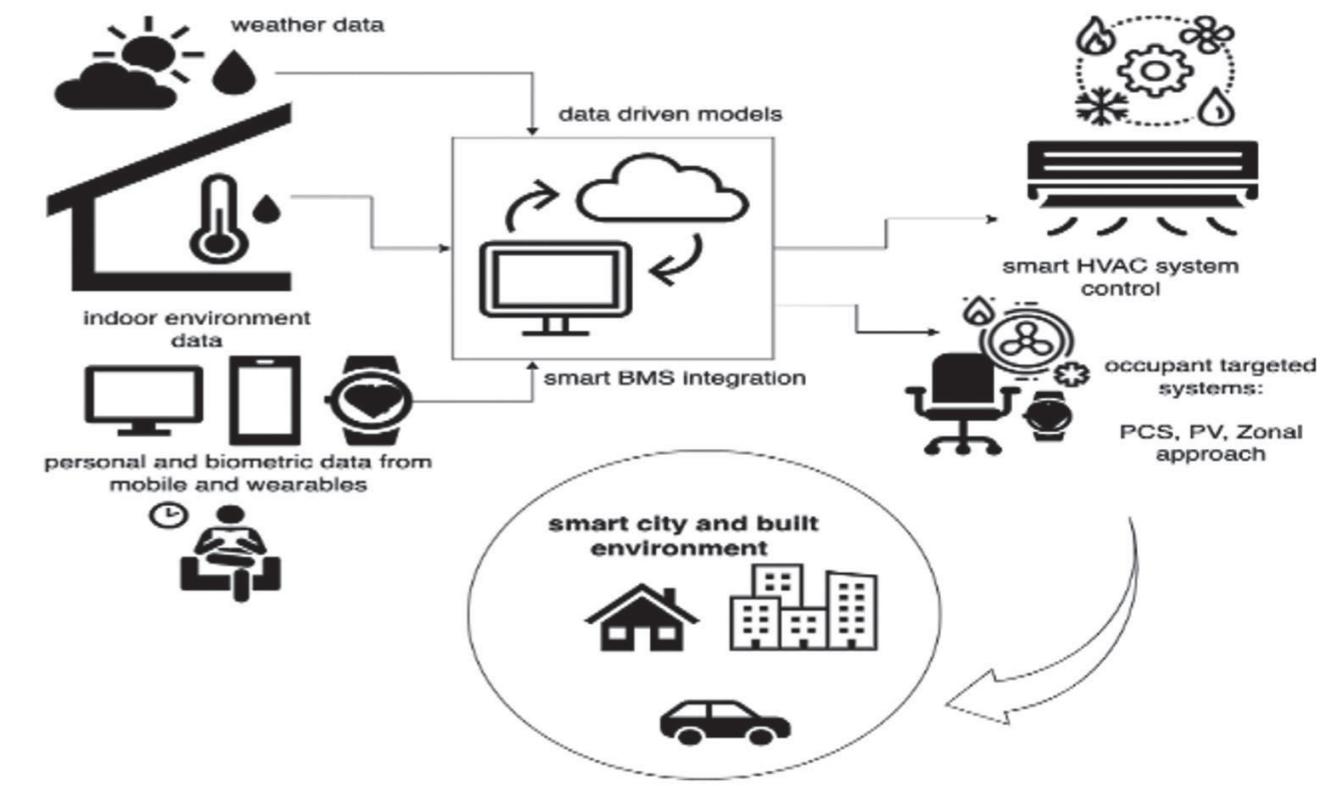


Fig.1. Concept of smart, user-centric, built environment

1. Heating and cooling where it is needed – Development of advanced Personalized ventilation (PV) and Personalized Comfort Systems (PCS) in correlation of the specific user needs in a human centric vision. In spite of the fact that users only utilize a small portion of the indoor space, the entire interior volume is heated or cooled to the same temperature from top to bottom, losing energy and producing unsatisfactory thermal wellbeing. Energy efficiency and thermal comfort may both be enhanced by personalized ventilation and personalized comfort systems. All PCS have a high impact on a person's thermal sensation while consuming little energy.

2. Advanced personal comfort systems (PCS) and their optimization - Individual perception difference of the thermal environment can account up to 2-3°C between persons. The actual paradigm of a one-size-fits-all (one setpoint temperature that should satisfy all occupants), used to control modern buildings with centralized mechanical systems is flawed. Diversity in thermal preferences underscores the need for an each-one-personal-size approach on one hand. On the other hand, the most influential body parts that affect the whole-body thermal sensation and the theory of alliesthesia, allow us based on the previous knowledge, to design and prototype new PCS.

3. Correlation models between real time thermal sensation and occupant behavioral patterns - Thermal sensation-based strategies considering a thermal indoor environment where the overall room tem-

Deep learning models based on data sets/typologies for predicting a user behavior pattern for the BMS to respond to the user needs – for instance based on new, hybrid adaptive thermal comfort models, allowing the correlation between the user needs and the outdoor environment. Personal comfort models are conceived to anticipate a single person's thermal comfort; as a result, they may not be directly relevant to other occupants. Repeatable patterns that can be applied to a bigger population may emerge as the size and diversity of the data grow. For instance, groups of models may come together to offer generic descriptions of thermal comfort that are applicable to population features (such as gender and age) or typical indoor spaces. The development of universal thermal comfort profiles can be based on these recurrent patterns. The profiles can be used for building/system design and operation to better characterize specific thermal comfort requirements across various segmentations of the building market, and they can serve as reasonable baseline models that can be easily applied to a new person who does not yet have a personal comfort model or whose personal comfort model is still under development.

Historical buildings management systems are dealing with special environments on which traditional models cannot be applied or might be extremely inefficient. Longitudinal data sets from real historical buildings can allow the development of new occupant-centric control strategies based on a new hybrid adaptive thermal comfort theory.

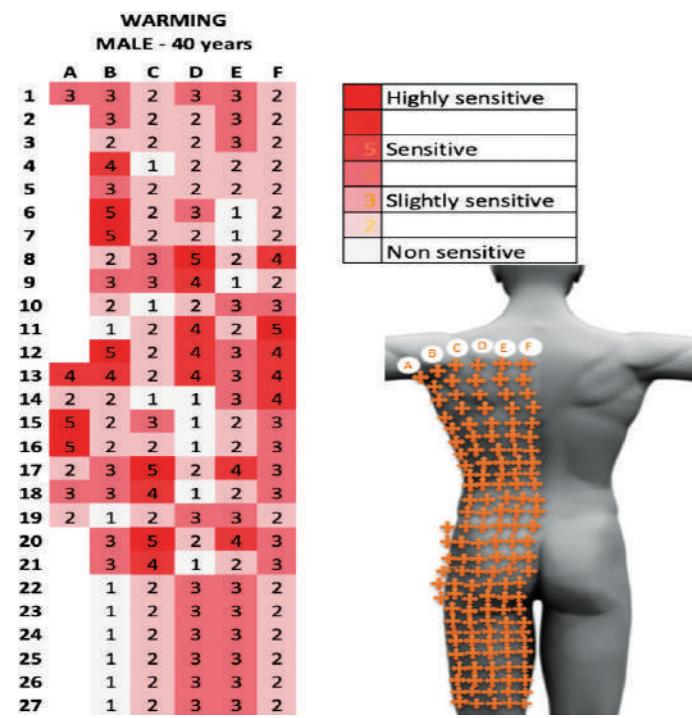


Fig.2. Example of thermal sensitivity distributions and the correlation of heating elements with thermal sensitivity zones (Nastase et al. 2022)

perature can fluctuate between much wider minimum and maximum temperatures and users get control over their own personal environment. Furthermore, the minimum (winter) and maximum (summer) temperatures are no longer fixed but are controlled according to occupant's real time sensations and the observed behavioral patterns.

Adaptive - Comfort - Control - Implemented Model (ACCIM), an emerging framework where heating and cooling setpoint temperatures of a building energy model are based on adaptive comfort models, seems to embody this newfound understanding. By integrating adaptive comfort models into building energy control, ACCIM potentially paves the way for

more energy-efficient and occupant-centered indoor climate regulation.

Such transformative potential warrants further research and validation, particularly in the context of building types and climates that were previously not considered in the scope of adaptive comfort models. The exploration of local adaptive comfort models and their energy implications, when compared with international models, could significantly contribute to this growing field of study. For instance, in Romania the 16798-1 N/A proposes a local adaptive comfort model developed by Udrea et al. (2018) and particularized for Bucharest region and office buildings.

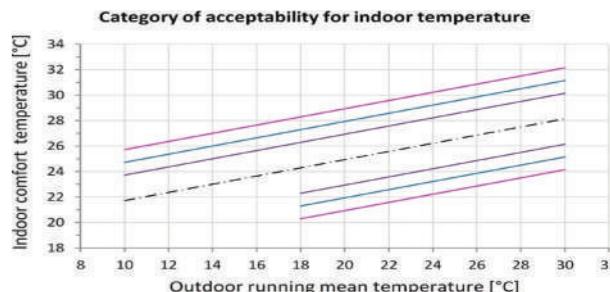


Fig.3. Adaptive thermal comfort equation for Romania (Udrea et al. 2018)

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HEAT EXCHANGERS

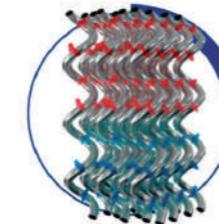

Economizoarele DNA ECO

Eficiență energetică în procesele de încălzire și transfer termic

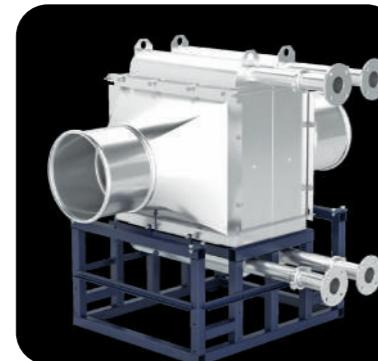
Aspectul mediului înconjurător cât și cel economic sunt importante în energetică (creșterea eficienței boilerelor pe gaz, recuperare și regenerare), precum și în procesele de producție generatoare de căldură reziduală (utilizarea căldurii reziduale generate de procesul tehnologic). Echipamentul standard pentru procesele de producție generatoare de căldură au de obicei un consum energetic ridicat, ducând la o încărcare semnificativă a mediului înconjurător și la o pierdere importantă de energie către atmosferă. Cu toate acestea, dacă ne concentrăm pe o eficiență mai ridicată a echipamentului, descoperim că o altfel de soluție are un impact pozitiv asupra mediului înconjurător.

DNA ECO reprezintă un produs derivat din binecunoscutul și apreciatul schimbător de căldură DNA cu fascicul tubular cu geometrie de helix. Această tehnologie atinge rate de transfer termic mult mai

ridicate comparativ cu soluția standard, permitând o construcție autoportantă și auto-compensatoare. Toate acestea aduc un mare avantaj când ne referim la suprafața de transfer termic și la hidraulică.



Curgerea turbulentă cu efect de vârtej crește coeficientul de transfer termic până la dublu mulțumită geometriei de helix a tuburilor. Suprafața de transfer termic mai eficientă cu distribuție omogenă a debitului și a vitezei de curgere. Fascicul tubular flexibil fără șicane, pierderi mici de presiune, fără nevoie de compensator pe manta și eliminarea vibrațiilor datorită multiplelor puncte de contact de-a lungul fasciculului tubular.



Fascicul tubular compus din tuburi cu geometrie de helix crează condiții extraordinare pentru dinamica fluidului. Mulțumită faptului că fascicul tubular nu are niciun plan de simetrie care să conecteze fiecare punct dintr-un tub, mediul creat ajuta la scăderea energiei disipate. Prin urmare debitul prin manta suferă pierderi de presiune mult mai mici. Rezultatul este o suprafață mare de transfer termic într-o construcție compactă.

Ultima generație a tehnologiei DNA ECO este un sistem modular complet din otel inoxidabil ceea ce oferă o soluție mult mai eficientă și adaptivă pentru multe aplicații de optimizare a recuperării energiei disipate.

Sistemul de module complet demontabile permite scoaterea și curățarea fiecărui segment de încalzire. Este echipat

cu izolație și sistem de distribuție, pregătit să fie conectat după boilere.

Cu toate acestea, este posibil să se livreze un singur modul la solicitarea clientului (unitate de transfer termic), facând posibilă extinderea sistemului după noile cerințe de transfer termic.



APLICAȚII

Recuperare caldură reziduală

- gaze arse de la boilerele pe gaz (arzătoare de gaz natural)
- gaze arse dintr-o altă sursă de energie (pro-pen-butan, lemn, biomasă)
- gaze reziduale rezultante din procese tehnologice
- azot, hidrogen, aer cald



TEHNOLOGIA DNA în procese tehnologice – Topirea aluminiului

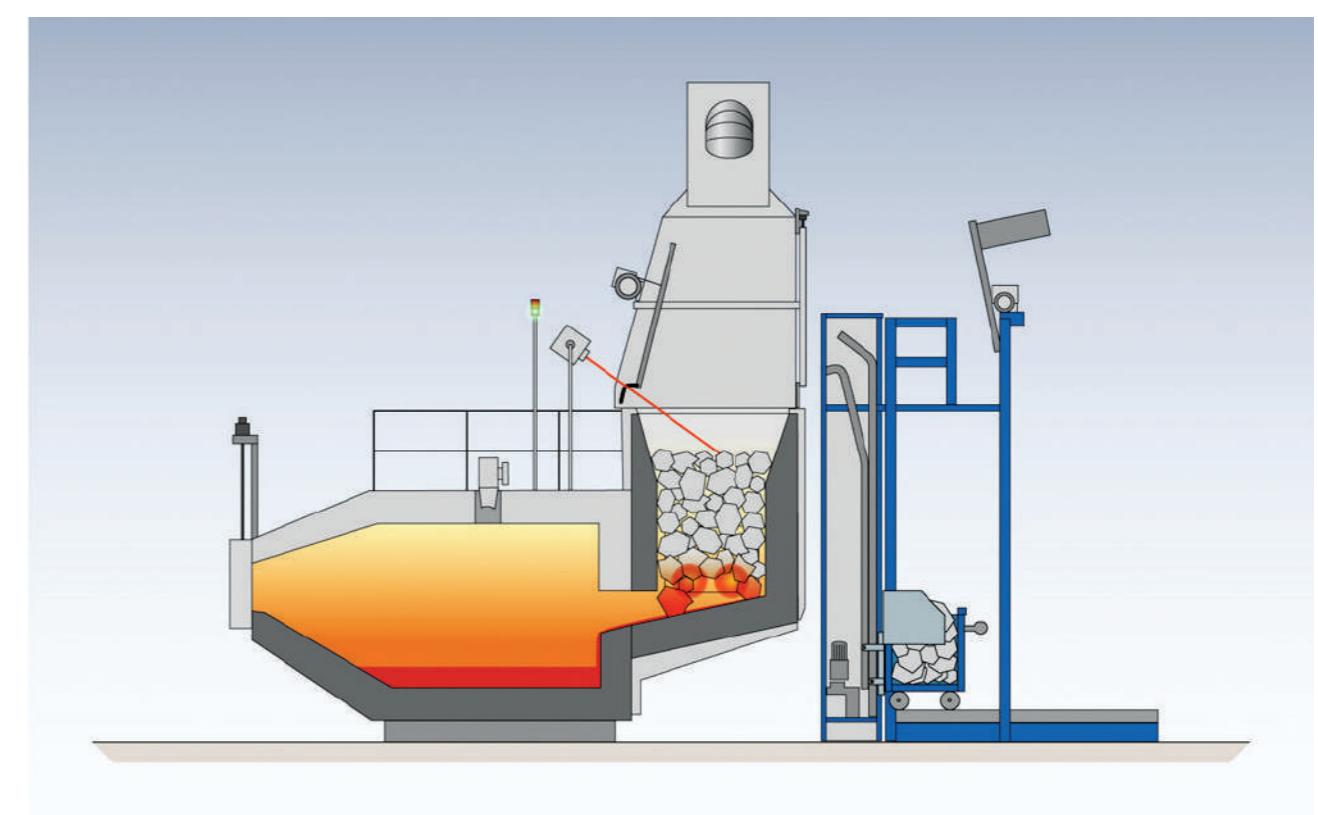
Idea de bază este folosirea energiei termice eliberate în aer drept caldură reziduală în urma procesului termic. De multe ori aceasta reprezintă o mare cantitate din energia utilizată în întregul proces de producție. Un exemplu de astfel de proces este topirea metalelor.

Unul dintre procesele cele mai mari consumatoare de energie este topirea aluminiului. În acest caz, în timpul procesului o cantitate importantă de energie e disipată în atmosferă sub formă de gaze arse fierbinți. În instalația existentă – un furnal cu o putere termică de 286 kW, debitul

de gaze arse poate fi determinat conform STN EN 734201, care în cazul nostru este de 0.1859 kg/s.

Când luăm în calcul temperatura gazelor arse și caldura specifică, obținem puterea termică a gazelor, care în cazul nostru este de 39 kW atunci când acestea sunt răcite de la 300°C la aproximativ 100°C. Această valoare arată pierderile economice survenite în urma procesului.

Cu tehnologia DNA ECO eficiența procesului e mult mai ridicată.





Guidelines on Investing in a Greener Future in Romania (Summary)

Raluca Teodosiu¹Mihai Tudorancea¹Andra Tanase^{1,2}¹UTCB (Technical University of Civil Engineering Bucharest)²TUD Group

Abstract

This study focuses on the thermal rehabilitation of 1,467 residential buildings in Bucharest. It aims to disseminate technical information and lessons learned from the project. The process involves a 10-step approach, including energy performance estimation, application for financing, and quality checks. The buildings collectively contain 99,332 apartments with a total developed area of 8,061,705 m². Data shows a significant decrease in energy consumption and CO₂ emissions after the rehabilitation, emphasizing the success and importance of such energy efficiency programs. This case study provides valuable insights for future green investments in Romania.

Keywords: energy efficiency, residential and public buildings, nZEB, reducing greenhouse gas



Introduction

Energy efficiency is one of the most essential components of current European policies and strategies. Therefore, reducing energy consumption is mandatory, taking into account the latest already-fixed target on CO₂ emissions limit both for existing and new buildings.

In this line on national level, several important rehabilitation programs are being out or are ongoing process on local administration strategy.

Taking into account our experience for the thermal rehabilitation of a pool of 1,467 (from 1682 included in Handbook) Owner's Associations for collective residential buildings from Bucharest, under monitoring process, the aim of this study is to disseminate technical information and more important learned lessons.

In accordance with this Handbook, from the beginning, a brief legislative summary is meant to underline the importance of the subject, followed by a short description of the buildings' situation before the implementation of rehabilitation works.

The main steps to be followed will inventory the successful implementation scheme. Issues from financial point of view will complete the picture as well as the learned lessons from those projects in order to conclude the thermal rehabilitation process.

Since 2007, TUD Group has been contributing to facilitate financing for the 1,467 Owner's Associations, mentioned above, but also to increase works' quality implementation through the monitoring task, both financially and technic.

Table 1. OA classification depending on year of construction

Year	≤4 floor	<4 floor	Total
1950-1960	67	44	111
1961-1970	176	228	404
1971-1980	182	260	442
1981-1990	264	238	502
1990-2005	1	7	8
Total OA	690	777	1,467

We will present the analysis of energy performance before and after the thermal rehabilitation for the above-mentioned pool. It is important to mention that the choice of OA presentation mode is due to the fact that the rehabilitation program is built depending on OA's request.

In this line, the energy performance is calculated according to the national methodology, taking into

Therefore, a success thermal rehabilitation program should follow the 10-step approach:

1. Inventory of existing building to be introduced in the program;
2. Energy performance estimations and possibility of reducing it in order to approve a local strategy through the local council;
3. Selection of the appropriate tender procedure type according to the potential of the buildings to be rehabilitated;
4. Application for financing resources;
5. Setup of main and quality characteristics to be requested in the tender procedure documentation, progress and award;
6. Technical design;
7. Quality design check and improving quality measures' implementation;
8. Execution of works;
9. Quality works' check and implementation of remedial measures;
10. Follow-up on works behavior and energy consumption during the guarantee period.

Usually, design and build procedure are mostly used, as well as separate design and separate build procedures. In order to increase the project's quality, the Fidic procurement contract type is to be considered. Concerning our pool, of buildings, the 1,467 Owner's Associations' buildings total 99,332 apartments with a total developed area of 8,061,705 m².

The collective residential buildings included in the analyzed pool are firstly categorized depending on 4 floors reference (according to legislative prescriptions), as presented in Table 1 (number of Owner's Associations' (OA) depending on year of construction:

account final energy consumption for heating, domestic hot water and artificial lighting.

Moreover, data calculated based on the MC001/2006 approach are extracted from energy performance certificates before, but also after, the thermal rehabilitation.

Accordingly, the energy performance before rehabilitation is presented in Table 2 such as:

Table 2. OA classification depending on energy performance before thermal rehabilitation

Specific final energy	≤4 floors	< 4 floor	Total
≤ 250 kWh/sqm y	156	257	413
251-300 kWh/sqm y	299	375	674
301-400 kWh/sqm y	223	143	366
< 401 kWh/sqm y	12	2	14
Total OA	690	777	1,467

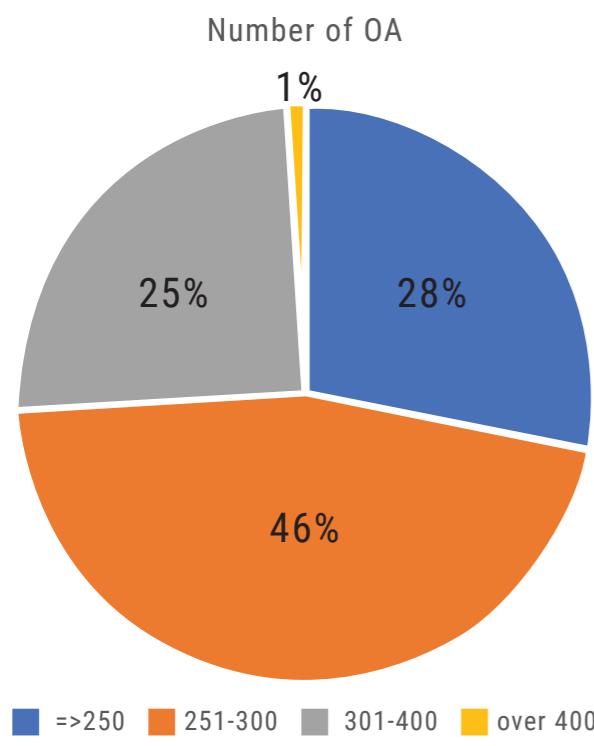


Fig. 1. Number of OA depending on energy performance before thermal rehabilitation

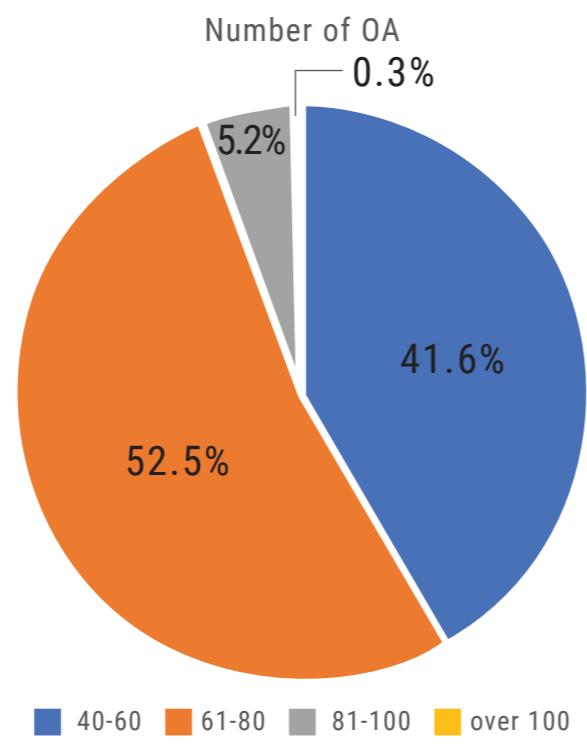


Fig. 2. Number of OA depending on CO₂ emissions before thermal rehabilitation

Taking into account that heating and domestic hot water are produced by the central district heating system and the electric energy is provided by national energy system, the specific CO₂ emissions, corresponding to the above-presented energy consumptions are grouped in Table 3.

Table 3. OA classification depending on CO₂ emissions before thermal rehabilitation

CO ₂ emissions	≤4 floors	< 4floor	Total
40-60 kg/sqm y	221	389	610
61-80 kg/sqm y	417	358	775
81-100 kg/sqm y	48	29	77
< 100 kg/sqm y	4	1	5
Total OA	690	777	1,467

The most important part of the buildings is characterized by a CO₂ between 61 – 80 kg/sqm y with a 53% from the total of 1467 OA. In Fig. 2 we present the percentage distribution of the analyzed buildings in order to better illustrate the environmental impact. After following the steps presented in the beginning, we focused our analysis on the energy performance after the implementation of thermal rehabilitation programs.

It is important to mention that the eligible categories of works for these residential buildings, according to the Romanian legislation are mainly: thermal insulation of outdoor walls, roof/terrace, over unhe-

ated basement slab, changing of windows, including closing balconies, rehabilitation of heating and domestic hot water distribution networks, as well as thermostatic valves for each radiator, changing of common areas artificial lightning or automatic balancing valves and directly related works. The results extracted from the energy performance certificates, after works, show an important decrease of energy consumption corroborated with the CO₂ emission mitigation.

In Table 4, we present the energy performance after the implementation of thermal rehabilitation works such as:

Table 4. OA classification depending on energy performance after thermal rehabilitation

	≤4 floors	< 4floor	Total
≤ 150 kWh/sqm y	298	411	194
151-200 kWh/sqm y	380	353	256
201-250 kWh/sqm y	12	13	25
Total OA	690	777	1,467
Total OA	690	777	1,467

In the same manner, the CO₂ emissions resulted after works are presented in Table 5 as follows:

Table 5. OA classification depending on CO₂ emissions after thermal rehabilitation

CO ₂ emissions	≤4 floors	< 4floor	Total
10-40 kg/sqm y	592	676	1268
41-60 kg/sqm y	95	101	196
61-80 kg/sqm y	0	0	0
< 81 kg/sqm y	3	0	3
Total OA	690	777	1,467

References

1. MC001 – Romanian Energy Performance Methodology, 2006
 2. OG18 – Government Ordinance 18, 2009, with subsequent additions and changes

Prezentul rezumat este inclus in volumul Conferintei RCEPB 2023, ISBN 978-606-25-0808-1, editat de MATRIX ROM si este publicat aici cu acordul editurii.



Thermal Bridges in the New Era of the NZEB and Passive Houses (Summary)



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Abstract

Implementation of the European environmental directives regarding the reduction of energy consumption during the use phase of buildings and CO₂ emissions, have led to the adoption of significant thicknesses for the thermal insulation of the opaque building envelope. Currently high-performance software and computing equipment is available. Yet often the modelling of the constructive details is done by "replacing" the effects of millimetre sized metal profiles with equivalent coefficients for thermal transfer. The analyses carried out, in which the modelling of the constructive details is in accordance with the constructive solution, show that even when an important thickness of performant insulating materials is used, the thermo-energetic effect of the thermal bridges is non-negligible..

Keywords: RCEPB, thermal bridges, thermal transfer.

Introduction

The latest technical norms in the field of the thermal bridges in Romania is the Mc001 - Annex K "Catalogue of thermal bridges", 2012. At that time we were talking about NZEB and passive houses that "will be". Until 2021 for housing design, the value of the corrected minimum resistance of external walls was 1.80 m²K/W (now we use 4.00 m²K/W for NZEB houses and 6.66 m²K/W for passive houses).

Due to the complexities they generate (the need to use high performance computing programs, operator qualification, long modelling time of a detail, etc.),

in most cases of thermal transfer, the details are modelled without describing the reinforcement in the case of reinforced concrete elements or thin metal profiles. Even if $\lambda_{\text{steel}} = 50 \text{ W/(mK)}$ and $\lambda_{\text{concrete}} = 1.60 \text{ W/(mK)}$, it is often considered that metal parts can be neglected due to their small size, the equivalent value being used for the composite product $\lambda_{\text{reinforced concrete}} = 1.74 \text{ W/(mK)}$. In the last decade, the adoption of high-performance thermo-energy insulation and with significant thicknesses, contributed to the "conservation" of the idea of using the equivalent permeability coefficients.

The applications analysed below aim to identify the differences of the results in the case of modelling using materials "with equivalent thermal permeability

"coefficients" and that of accurate modelling of the details. A number of details considered to be representative from the point of view of the analyzed issue will be presented.

Case 1: Outer angle between 25 cm thick walls made of full bricks with ETICS - 10 cm m.w.

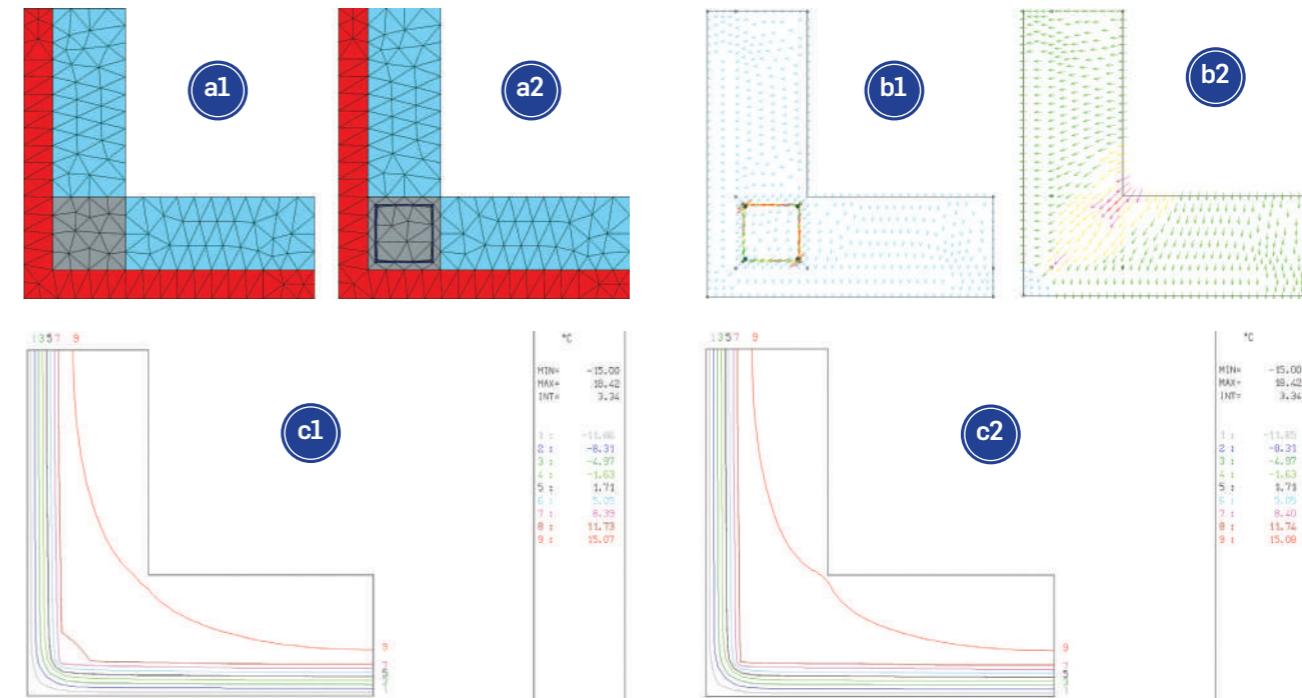
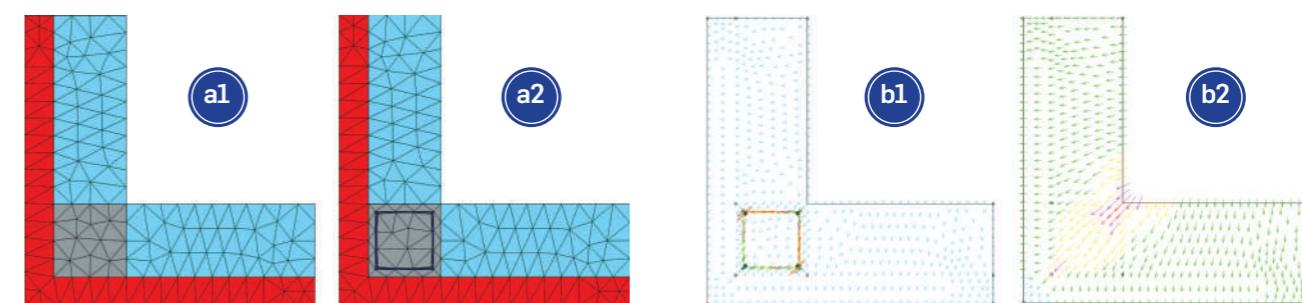


Fig.1. Outer angle between 25 cm thick walls made of full bricks, with ETICS
1) solution without reinforcement; 2) solution with reinforcement;
a) finite element modelling; b) heat flow direction; c) isothermal field;

Tab. 1. Thermal analysis values

Modelling	Φ	$\theta_{\text{si,min}}$
	(W)	(°C)
solution without reinforcement	10.22	15.90
solution with reinforcement	10.44	15.55

Case 2: Outer angle between 25 cm thick walls made of full bricks with ETICS - 10cm m.w., dowel pin, in contact with the reinforcement



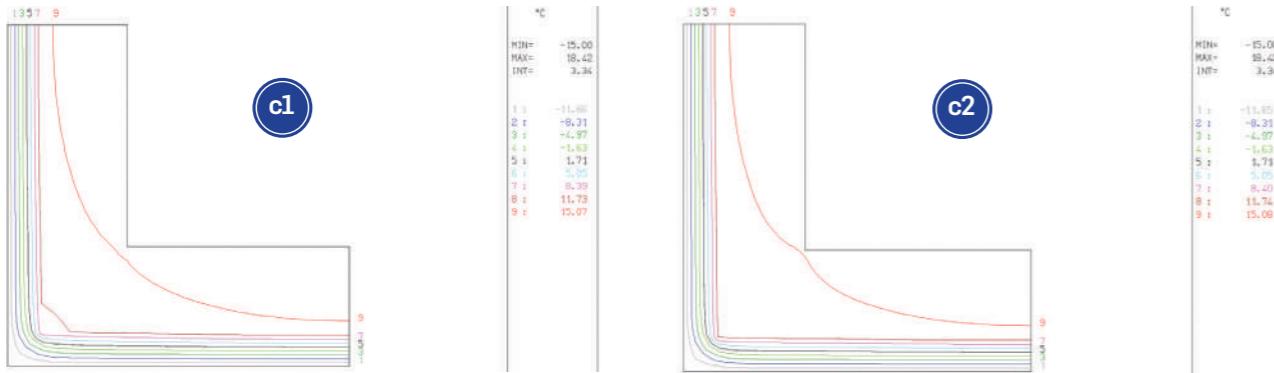


Fig.2. Outer angle between 25 cm thick walls made of full bricks, with ETICS, dowel pin, in contact with the reinforcement
1) solution without reinforcement; 2) solution with reinforcement and dowel pin;
a) finite element modelling; b) heat flow direction; c) isothermal field;

Tab. 2. Thermal analysis values

Modelling	Φ	$\theta_{si,min}$
	(W)	(°C)
solution without reinforcement	10.22	15.90
solution with reinforcement and dowel pin, in contact with the reinforcement	18.25	10.21

For details of intersection between slabs and outer walls, connection infrastructure – outer wall, building with basement, connection between exterior walls and "last" slab (terrace roof) etc. the differences between the models without reinforcement and reinforcement, increase.

Even if $\lambda_{metal} \approx 50 \text{ W/(mK)}$ and $\lambda_{concrete} = 1.60 \text{ W/(mK)}$, relying on the fact that the metal parts are embedded in the reinforced concrete elements, for the practical "speed" equivalent characteristics of the composite material are often used: $\lambda_{reinforced concrete} \approx 1.74 \text{ W/(mK)}$. These give rise to local thermal bridges, often unfavourable.

Following the analyses carried out, the following conclusions were formulated:

- there are important differences (about 40 ... 50%) in terms of thermal flows, between the analysed cases (without external thermal system) with reinforcement on the outer face (prefabricated panels) and the modelling without considering the reinforcement;

- when we analyse the cases with external thermal system, we can see that there are no important differences in the level of the thermal flows (about 3 5%), between the cases with and those without reinforcement;
- between the models with and those without metal dowel anchoring of the external thermal system, there are significant differences (approx. 40%) in the thermal flow;
- if the metal anchor bolt of the thermal system is in contact with the reinforcement, the differences increase even more than in the previous case;
- the computed differences in terms of coefficients of thermal losses are extremely varied; differences in the internal temperature can reach up to 1°C;

Consequently, it is appreciated that for a correct and complete thermo-energetic analysis of a constructive detail, it is necessary to use the calculation programs that allow the modelling of the details according to the real solution.

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