

EFFICIENCY
IN CONSTRUCTIONS



DEMAND MORE! CHOOSE ONLY THE BEST.

AAC masonry - innovation for efficient homes

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ORAȘUL VIITORULUI SE CONSTRUIEȘTE CU CELCO

CELCO S.A.

With a **tradition spanning over more than 40 years**, CELCO is among the first companies producing ACC (autoclaved cellular concrete), lime, adhesives and mortars.

CELCO is a **100% Romanian company** and stands for products manufactured in Romania, these being increasingly appreciated, both in the country and abroad.

2020

DDI CELCO

FIU PREȚENTIOSI ALEGEȚI PE CEL MAI BUN.

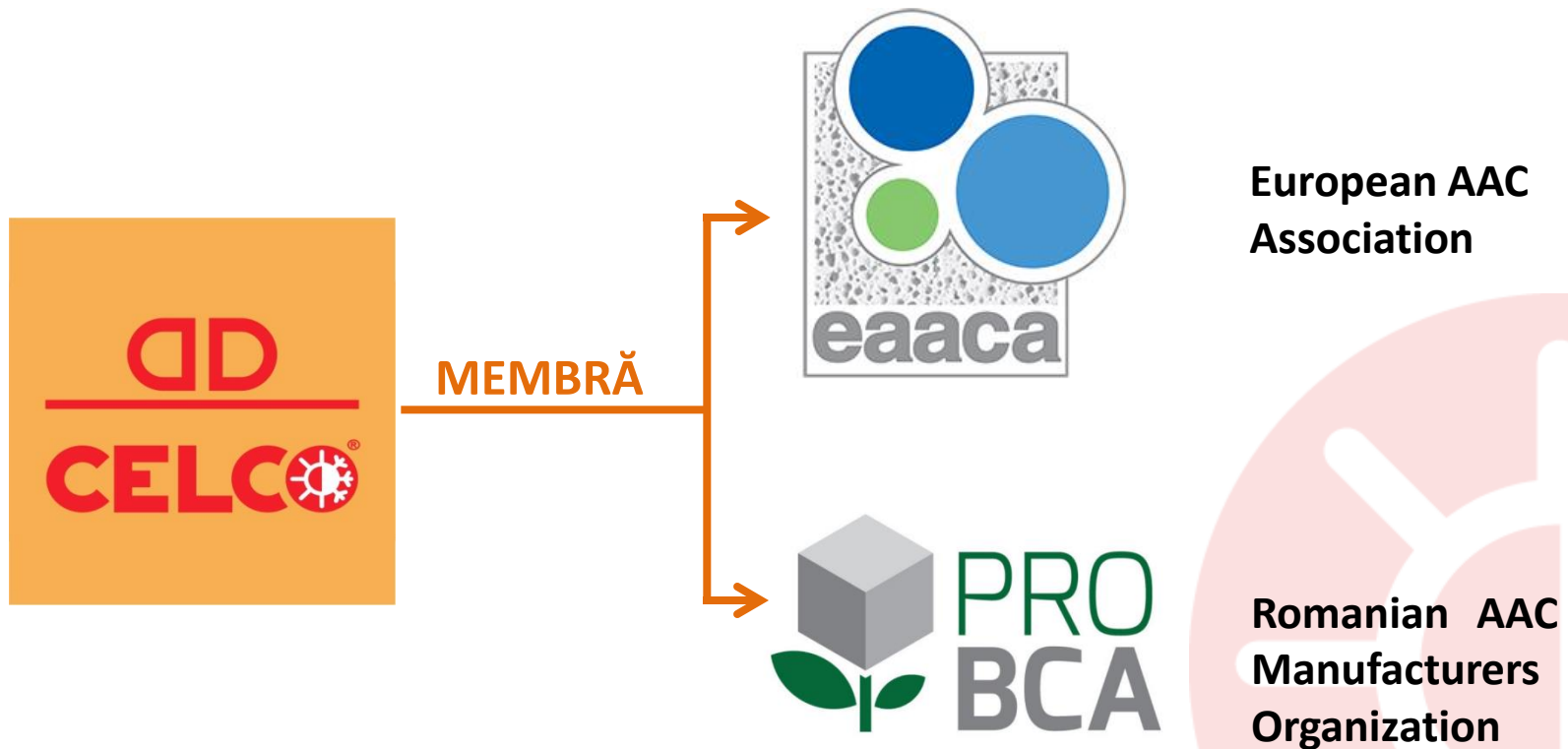


The company is part of a large group of companies operating in key areas of the Romanian industry (cumulative 2017 turnover: approximately 45 million Euros).



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CELCO is involved at national and European level in promoting the AAC as a modern and efficient solution.



2020 Strategy

In order to be in line with the 2020 strategy, new buildings must be **nZeB** (near zero energy buildings) = buildings with almost zero energy consumption.

How do we build a nZEB building?

- High degree of insulation;
- Effective window systems;
- High-efficiency sealing and natural / mechanical ventilation with a heat recovery system to reduce heating / cooling needs.

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- Buildings are currently responsible for **40%** of primary energy consumption.
- There is an energy saving potential in the EU of **20-50%**.
- The **building's energy performance** refers to the total annual energy needs that includes heating, cooling, hot water, electricity.



Improvement of the efficiency of buildings is much easier to achieve in the design phase rather than refurbishing older buildings.

- Norms MC 001/1 "Methodology for calculating the energy performance of buildings" and C107 "Thermotechnical calculation in construction" **are obsolete!**

Arguments:

- Cellular concrete production technology has gone through major progress in recent years;
- The current versions of these documents present in Appendix A properties of ACC products that are currently no longer found on the market;
- It is necessary to **update the values** according to the tests performed on the new improved ACC products.

0	1	2	3
65	Zidărie din cărămizi de diatomit, cu densitatea aparentă a cărămizilor de 1000 kg/m ³	1200	0,52
66	Zidărie din blocuri mici pline din beton cu agregate ușoare, cu densitatea aparentă a blocurilor de:		
	2000 kg/m ³	1980	1,16
	- 1800 kg/m ³	1800	0,93
	- 1600 kg/m ³	1620	0,75
	- 1400 kg/m ³	1440	0,61
	- 1200 kg/m ³	1260	0,50
	- 1000 kg/m ³	1080	0,42
67	Zidărie din blocuri de beton celular autoclavizat:		
	- cu rosturi subțiri		
	- tip GBN 35	675	0,27
	- tip GBN 50	775	0,30
	- cu rosturi obișnuite		
	- tip GBN 35	725	0,30
	- tip GBN 50	825	0,34
68	Fâșii armate din beton celular autoclavizat	625	0,25
	- tip GBN 35	725	0,28
	- tip GBN 50		

3. Pentru materialele care nu sunt cuprinse în anexa A, conductivitatea termică se poate determina experimental, conform STAS 5912-89 (pentru materialul în stare uscată), conductivitatea fiind raportată la temperatura medie de 0°C.

Conductivitățile termice de calcul λ se obțin prin majoritatea valorilor determinate experimental λ_0 după cum urmează:

- betoane ușoare având:

$\lambda_0 \leq 0,16$ W/(mK) 60%

$\lambda_0 = 0,17 \dots 0,23$ W/(mK) 35%

$\lambda_0 = 0,24 \dots 0,30$ W/(mK) 30%

$\lambda_0 = 0,31 \dots 0,46$ W/(mK) 25%

$\lambda_0 = 0,47 \dots 0,58$ W/(mK) 20%

- produse din vată minerală 10%

produse din lemn 20%

- produse fibroase de natură organică 20%

- masă ceramică 20%

- polimeri și spume din polimeri

- cu pori închiși 10%

cu pori deschși 20%

4. Densitatea aparentă dată în anexa A, se referă la materialele în stare uscată până la masă constantă.

5. Pentru materiale cuprinse în anexa A, dar având alte densități aparente, conductivitatea termică de calcul se poate determina prin interpolare.

6. Pentru materialele și densitățile aparente necuprinse în anexa A, coeficientul de asimilare termică s se calculează conform pct. 12.4 din prezentul normativ.

7. Pentru materialele care nu au valori $1/K_D$ în anexa A, precum și pentru alte materiale necuprinse în anexa A, factorul rezistenței la permeabilitate la vapori se va determina pe cale experimentală de către un institut de specialitate.

8. Pentru materiale sub formă de vopsale, pelicule sau folii, valorile $1/K_D$ se dau în STAS 6472/4-89.

Through PRO BCA, proposals were made to MDRAP (Ministry of Regional Development and Public Administration) **to update Appendix A** and modify the conversion factor of $\lambda_{10,dry}$ in $\lambda_{calculation}$, according to the following argumentation:

- 1) We consider that in the above-mentioned norms it is necessary to specify as the first option the choice and calculation of the individual product values by the design engineer based on the data provided by the manufacturers in the **Declaration of Performance**.

- 2) The updated Appendix A (identical in both norms) **must contain the full range of densities** of the currently used ACC elements and the correct thermal conductivity.

0	1	2	3	4	5
12	Beton cu granulit	1800 1700 1600 1500 1400 1200 1000 800 600 400	0,81 0,76 0,70 0,64 0,58 0,46 0,35 0,29 0,23 0,17	9,41 8,85 8,24 7,63 7,02 5,79 4,61 3,75 2,89 2,03	7,1 7,0 6,9 6,8 6,5 6,1 4,7 3,4 2,4 1,9
13	Beton celular autoclavizat (gazbeton): -tip GBC - 50 -tip GBN - 50 -tip GBN - 35 -tip GBN - T; GBC - T	750 700 600 550	0,28 0,27 0,24 0,22	3,57 3,39 2,96 2,71	4,2 4,2 3,7 3,5
14	Produse rigide spumate din cenușă de termocentrală liată cu ciment	500 400	0,20 0,16	2,46 1,97	3,1 2,6
IV Mortare Capacitate calorică masică c=840 J/(kgK)					
15	Mortar de ciment	1800	0,93	10,08	7,1
16	Mortar de ciment și var	1700	0,87	9,47	8,5
17	Mortar de var	1600	0,70	8,24	5,3
18	Mortar de zgură cu ciment	1400 1200	0,64 0,52	7,37 6,15	5,7 4,7

We hereby propose the real values of thermal conductivity in the following table:

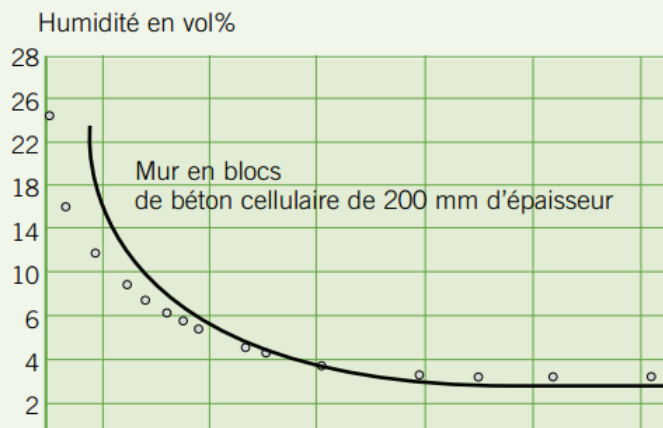
Dry density kg/cbm	$\lambda_{10',dry}$ (EN 1745) W/m° K		PROBCA graph	$\lambda_{10',dry}$ proposal
	P=50%	P=90%		
300	0.072	0.085	0.088	0.08
400	0.096	0.11	0.108	0.11
500	0.12	0.13	0.132	0.13
600	0.15	0.16	0.152	0.15
700	0.17	0.18	0.172	0.17

3) Modification of conversion factor of $\lambda_{10,dry}$ in $\lambda_{calculation}$

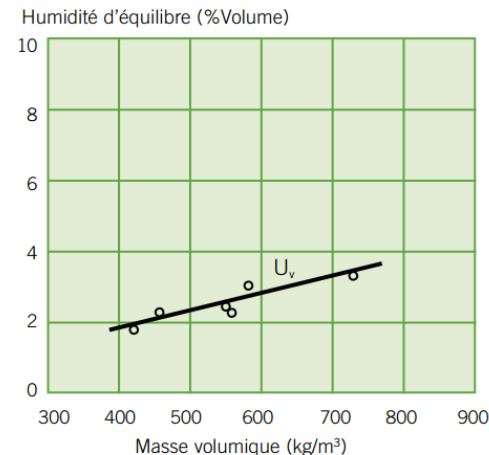
The C107 / 1 norm and the calculation methodology impose that for $\lambda_0 \leq 0,16 \text{ W / m}^\circ \text{ K}$ the applied correction is 60% (i.e. a conversion factor of 1.6), taken from the norms of the 1980s, which we considered incorrect in the case of current autoclaved cellular concrete.

We extract from the literature provided by associations of ACC producers in Belgium and Germany

Courbe de séchage des blocs en béton cellulaire à température ambiante intérieure [24]



Teneur en humidité d'équilibre (en volume) en fonction de la masse volumique [22]



We extract from the literature provided by associations of ACC producers in Belgium and Germany

Abb. 6.2: Trocknungsverlauf von Porenbeton-
außenbauteilen

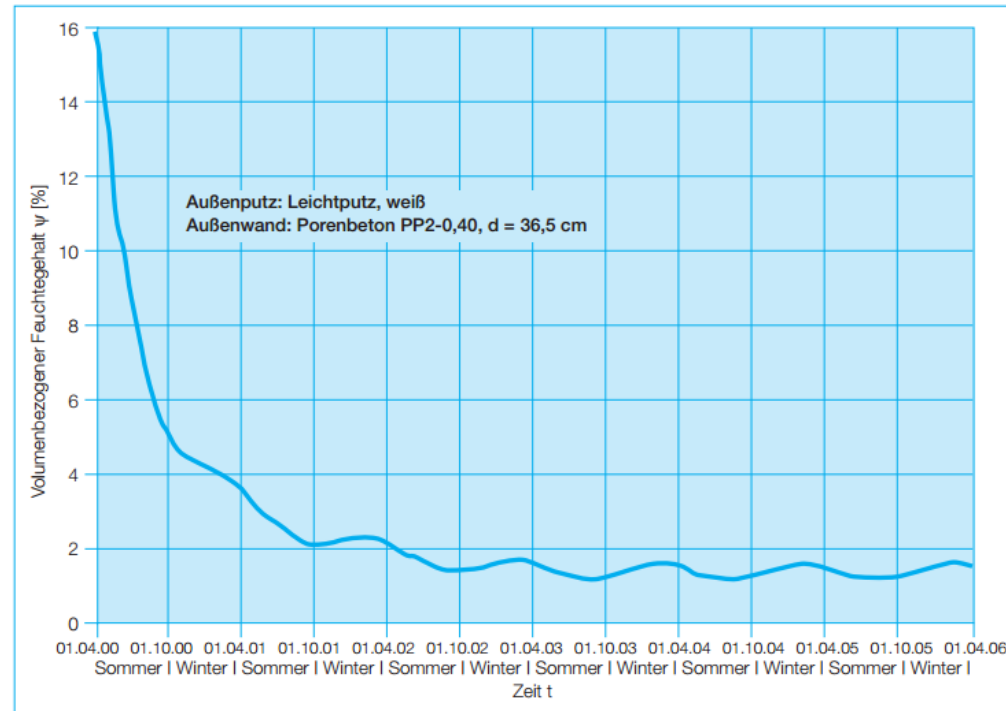
Thus, it results that the humidity of ACC products decreases over time to a constant humidity, with the final conversion factor being 1.1.

The EN 1745 standard indicates the following conversion relationship:

$$\lambda_{\text{calculation}} = \lambda_{10, \text{dry}} \times e^{\text{fu} \times U_{\text{calculation}}}$$

The Norm MP 022-02 "Methodology for the evaluation of the thermotechnical performance of building materials and products" indicates the following calculation relation for the conversion of the thermal values:

$$\lambda_2 = \lambda_1 \cdot F_T \cdot F_w$$



Klimarandbedingungen: Innen $\theta = 20^\circ\text{C}$ und $\phi = 50\%$, außen Standort Essen

Bundesverband Porenbeton - Germania

http://bv-porenbeton.de/attachments/article/44/Handbuch_Porenbeton_2008.pdf

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In Annex D of **MP 022-02 norm**, the moisture content values for AAC are given.

**PROPRIETĂȚI ALE UNOR MATERIALE ȘI PRODUSE
PENTRU CONSTRUCȚII**
– umiditatea la echilibru higrotermic cu aer atmosferic –

Nr. crt.	Materialul	Densitatea materialului în stare uscat	Umiditatea absolută masică a materialului la echilibru cu aer la 23°C și 50 %		Umiditatea absolută masică a materialului la echilibru cu aer la 23°C și 80 %		Coeficientul de conversie pentru umiditate	
			Umiditatea relativă		Umiditatea relativă			
			w_w	w_r	w_w	w_r	$f w_w$	$f w_r$
		kg/m ³	kg/kg	m ³ /m ³	kg/kg	m ³ /m ³	–	–
1.	2.	3.	4.	5.	6.	7.	8.	9.
1.	Ceramică arsă	1000-2400	–	0,007	–	0,012	–	10
2.	Silico-calcare	900-2200	–	0,012	–	0,024	–	10
3.	Beton celular autoclavizat	300-1000	0,026	–	0,045	–	4	–
4.	Mortar (de zidărie și tencuială)	250-2000	–	0,04	–	0,06	–	4

$u_{23^{\circ}\text{C}, 50\%} = 0.026$ moisture content of the masonry material in air balance at 23 ° C and relative humidity of 50%

$u_{23^{\circ}\text{C}, 80\%} = 0.045$ moisture content of the masonry material in air balance at 23 ° C and relative humidity of 80%.

By interpolation we calculate $u_{23^{\circ}\text{C}, 65\%} = 0.036$

For mortars: $u_{23^{\circ}\text{C}, 50\%} = 0.04$; $u_{23^{\circ}\text{C}, 80\%} = 0.06$, and by interpolation $u_{23^{\circ}\text{C}, 65\%} = 0.05$

For the values of the thermal conductivity calculations of the ACC masonry we read section 7.2.3. of C107-205 part 3 for the calculation of the equivalent thermal conductivity of the ACC masonry, taking into account the thermal conductivity of the ACC product, the thermal conductivity of the mortar and the area of the quasi-homogeneous layer components measured in the plane of the layer (in elevation).

$$\lambda_{ech} = \Sigma (\lambda_j \times A_j) / \Sigma A_j.$$

The calculations made with these data are centralized in the following tables, mentioning that an 80% humidity of the environment is not found under normal operating conditions of the building (only in exceptional cases, for short periods of time). The normal conditions we propose to include in the norm for a relative humidity of 50% / max. 65% .

We propose updating the Annex A and modification of conversion factor of $\lambda_{10,dry}$ in $\lambda_{calculation}$, according to the following argumentation:

AAC density (kg/cbm)	λ_{calcul} (W/m°K) AAC element		λ_{calcul} (W/m°K) mortar		λ_{ech} (W/m°K) Thin joint AAC masonry		λ_{ech} (W/m°K) Normal joint AAC masonry	
	23 C 50%	23 C 80%	23 C 50%	23 C 80%	23 C 50%	23 C 80%	23 C 50%	23 C 80%
300	0.09	0.10	0,94	1.03	0.10	0.11	0.13	0.14
400	0.12	0.14	0,94	1.03	0.13	0.15	0.16	0.18
500	0.15	0.16	0,94	1.03	0.16	0.17	0.19	0.20
600	0.17	0.19	0,94	1.03	0.18	0.20	0.21	0.23
700	0.19	0.21	0,94	1.03	0.20	0.22	0.22	0.25

We propose updating the Annex A and modification of conversion factor of $\lambda_{10,dry}$ in $\lambda_{calculation}$, according to the following argumentation:

AAC density (kg/cbm)	λ_{calcul} (W/m°K)	λ_{calcul} (W/m°K)	λ_{ech} (W/m°K)	λ_{ech} (W/m°K)
	AAC elements	mortar	Thin joint AAC masonry	Normal joint AAC masonry
	23 C	23 C	23 C	23 C
	65%	65%	65%	65%
300	0.09	0,98	0.10	0.13
400	0.13	0,98	0.14	0.17
500	0.15	0,98	0.16	0.19
600	0.18	0,98	0.19	0.22
700	0.20	0,98	0.21	0.24

The PRO BCA members have made through experimental laboratories **URBAN-INCERC IASI Branch**, new experimental determinations of stationary thermal transfer properties on a real scale model for two types of masonry made of AAC elements with a thickness of 35 cm and 37,5 cm.

- 1) The average thermal conductivity at 10°C of the dry ACC blocks used to build the physical model was determined to the value of: **$\lambda_{10 \text{ med dry}} = 0,106 \text{ W/mK}$**
- 2) Average apparent dry density, determined on 4 blocks of each type: **$\rho_i = 405,18 \text{ kg/m}^3$**
- 3) Thermal transfer resistance
 - total thermal resistance of the wall in 350 mm ACC blocks **$R_{T-350} = 3,337 \text{ m}^2\text{K/W}$**
 - total thermal resistance of the wall in 375mm ACC blocks **$R_{T-350} = 3,458 \text{ m}^2\text{K/W}$**
- 4) The equivalent thermal conductivity coefficient (λ_{ech})
 - equivalent thermal conductivity of dry masonry, in 350mm ACC blocks **$\lambda_{\text{ech } t \text{ 350}} = 0,1049 \text{ W/mK}$**
 - equivalent thermal conductivity of dry masonry, in 375mm ACC blocks **$\lambda_{\text{ech } t \text{ 375}} = 0,1084 \text{ W/mK}$**

0	1	2	3	4	5
65	Zidărie din cărămizi de diatomit, cu densitatea aparentă a cărămizilor de 1000 kg/m ³	1200	0,52	6,26	3,4
66	Zidărie din blocuri mici pline din beton cu agregate ușoare, cu densitatea aparentă a blocurilor de:				
	- 2000 kg/m ³	1980	1,16	12,02	10,6
	- 1800 kg/m ³	1800	0,93	10,26	8,5
	- 1600 kg/m ³	1620	0,75	8,72	7,1
	- 1400 kg/m ³	1440	0,61	7,43	4,7
	- 1200 kg/m ³	1260	0,50	6,29	4,3
	- 1000 kg/m ³	1080	0,42	5,34	3,9
67	Zidărie din blocuri de beton celular autoclavizat:				
	- cu rosturi subțiri				
	- tip GBN 35	675	0,27	3,38	3,8
	- tip GBN 50	775	0,30	3,82	4,3
	- cu rosturi obișnuite				
	- tip GBN 35	725	0,30	3,70	3,9
	- tip GBN 50	825	0,34	4,20	4,4
68	Fășii armate din beton celular autoclavizat				
	- tip GBN 35	625	0,25	3,13	3,7
	- tip GBN 50	725	0,28	3,57	4,2

New buildings with monolayer exterior masonry made of CELCO ACC of **min. 35 cm** are energy efficient because they limit heat loss and do not need extra insulation!



**Some of our customers' fears
which we have managed to
effectively contradict, regarding AAC:**

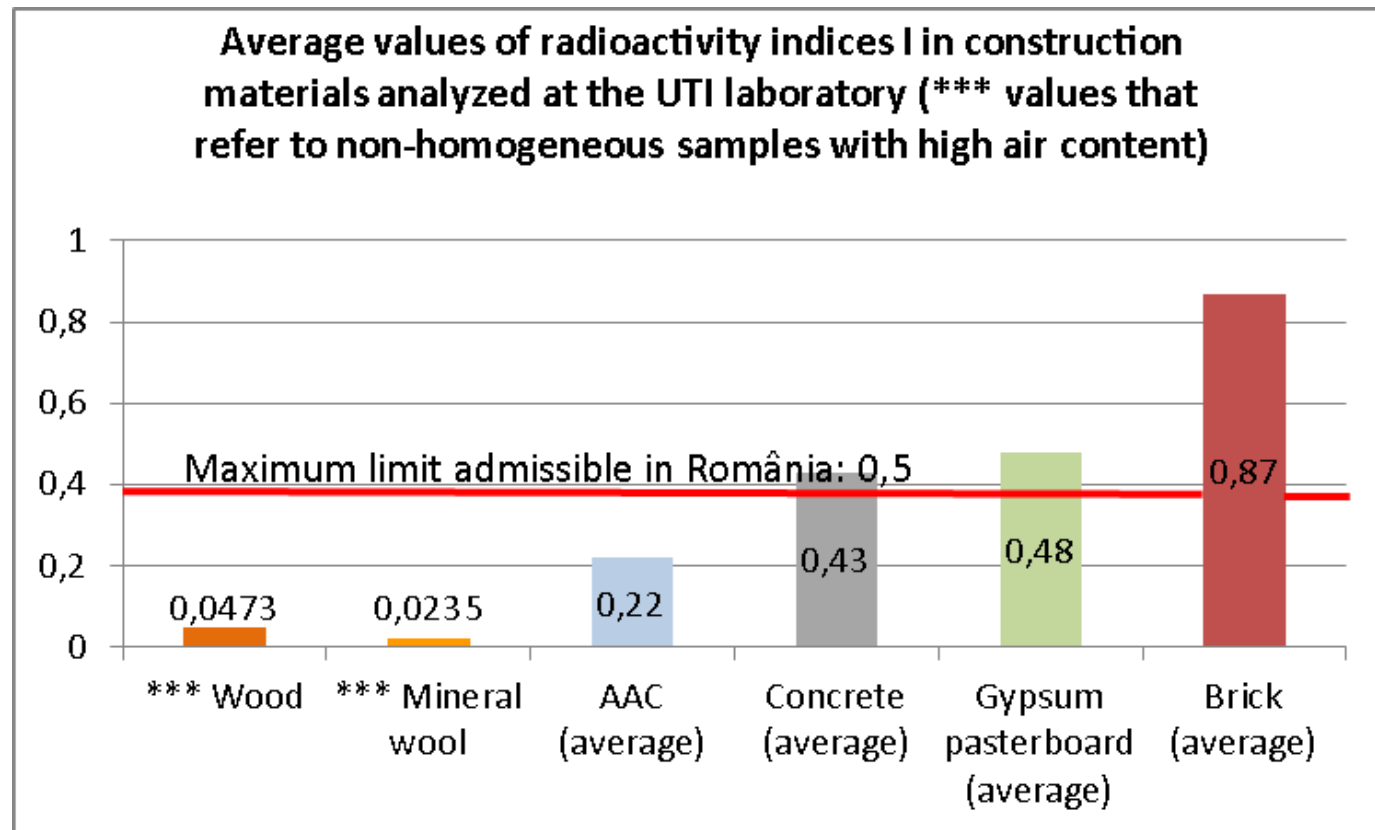
- Radioactivity of building materials;
- Fire resistance of building materials

➤ **CELCO ACC is a healthy material:**

The phenomenon of radioactivity is present naturally everywhere, being called natural radioactivity. Thus, radionuclides are found in rocks, air, water, soil and in living organisms, including humans..

Most people spend 80% of the time inside buildings, therefore it is important that natural radioactivity from building materials falls within the permissible limits.

* Research results by the **Technical University of Iasi, 2015**



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Why choose CELCO AAC?

➤ **With CELCO AAC you get a fire resistant building:**

CELCO ACC is 100% non-combustible, meets **Euroclass A1** requirements for **fire reaction**, does not burn or loses its compressive strength for **at least 4 hours**, does not release toxic fumes and prevents the spread of fire.



Foto 9 – Distribuția temperaturii pe fața neexpusă la foc a epruvetei în minutul 180 al încercării de rezistență la focul standard

II. În conformitate cu prevederile contractului nr. 7253 din 10.10.2016, încheiat între INCD „URBAN-INCERC” și “CELCO S.A.”, cu denumirea: *Cercetări experimentale privind determinarea rezistenței la foc pentru elemente de zidărie din BCA, cu dimensiunile 625 mm × 250 × 240 mm și densitate în stare uscată 400±30 kg/mc, pentru grosime zid 250 mm, s-a întocmit Raportul de cercetare nr. 6 din 15.02.2017: II. Cercetări experimentale privind determinarea rezistenței la foc pentru elemente de zidărie din BCA fabricate de “CELCO S.A.”.*

Pe baza rezultatelor obținute în urma încercării de rezistență la foc a epruvetei alcătuită din elemente de zidărie din BCA, vă comunicăm următoarele informații:

Epruveta testată la rezistența la foc, are următoarele caracteristici:

Tabel 3

Dimensiuni de ansamblu epruvetă		Alcătuirea epruvetei		
L×H (mm)	Grosime (mm)	Dimensiuni elemente din BCA fabricate de CELCO S.A. 625×250×240 mm	Densitate elemente din BCA fabricate de CELCO S.A. 400±30 Kg/mc	Mortar folosit la țeserea elementelor din BCA Mortar pentru zidărie BCA cu straturi subțiri M10 de la firma CELCO S.A.
3000 × 3000	250			

Epruveta a fost testată conform SR EN 1363-1:2012 și SR EN 1364-1:2015 iar durata de expunere la acțiunea focului a fost de **245 de minute**. Rezultatele încercării de rezistență la foc conform cerințelor prevăzute în SR EN 13501-2+A1:2010 sunt prezentate în tabelul 4:

PROJECTS WITH CELCO AAC



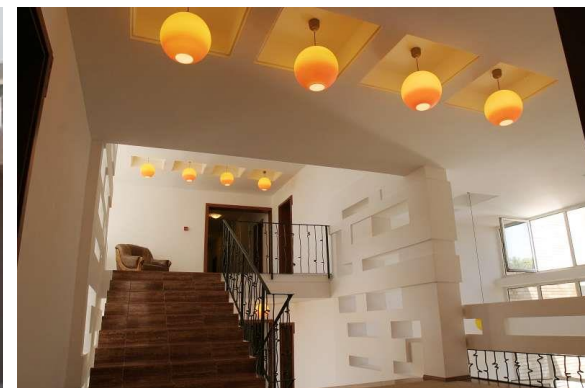
**ALMAR Constanța
Business Center**



Apart Hotel Mamaia



Hotel 2D Neptun



**Tomis Business
Center Constanța**



Summerland Mamaia



Hotel Scapino Mamaia
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PROJECTS WITH CELCO AAC



Apartments building



Lira Residence Constanța



Nord Residence



Solid Residence Mamaia



CELCO

OHSAS 18001:2007



Occupational Health and
Safety Management System

ISO 9001:2008



Quality Management System

ISO 14001:2005



Environmental Management System

EFFICIENCY
IN CONSTRUCTIONS



DEMAND MORE! CHOOSE ONLY THE BEST.

AAC masonry - innovation for efficient homes

Irina Odor – Commercial Manager

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